



Sheltering effect of various wave energy converter archetypes in arrays

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Background → Wave Sheltering

Offshore structures and coastlines face **fatigue damage and deterioration** due to cyclical wave loads^{[1],[2]}

Wave energy converters (WECs) extract power from ocean waves, leaving **lower energy waves in their wake**

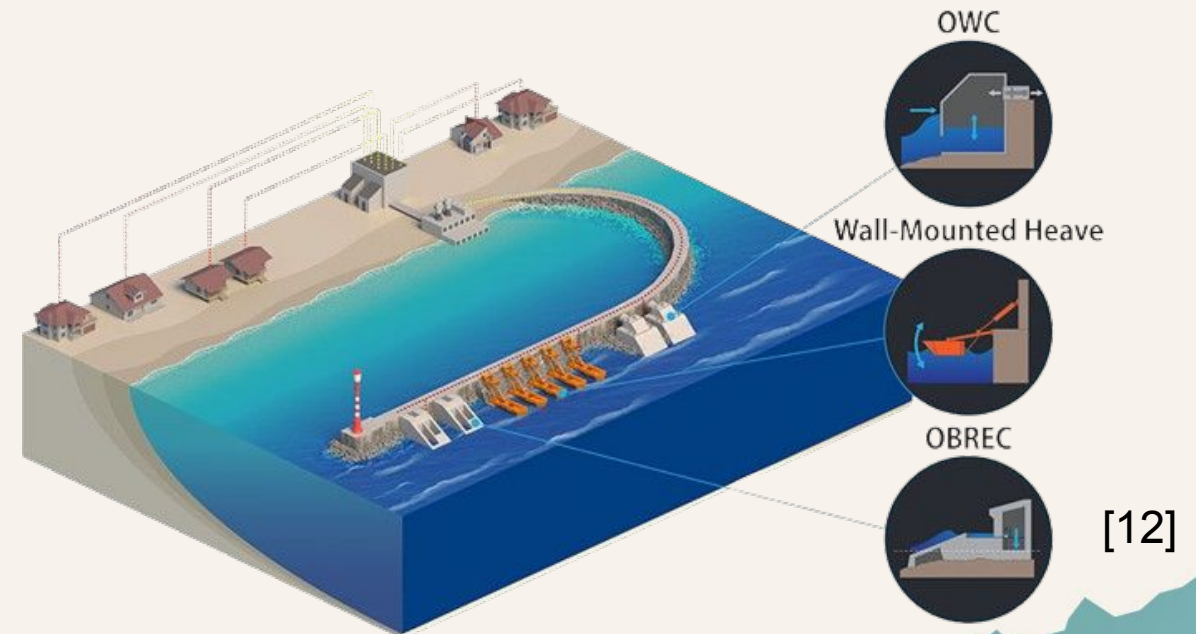


Background → Wave Sheltering

Studies have investigated the **wave sheltering capabilities of different WECs** for protecting vulnerable coastlines^{[4],[5],[6],[7]}, offshore aquaculture farms^[8], and offshore wind installations^{[9],[10],[11]}

NREL^[12] is working to construct **coastal structure integrated WECs**, which are attached to traditional fixed breakwaters

This presentation focuses specifically on **floating WECs**



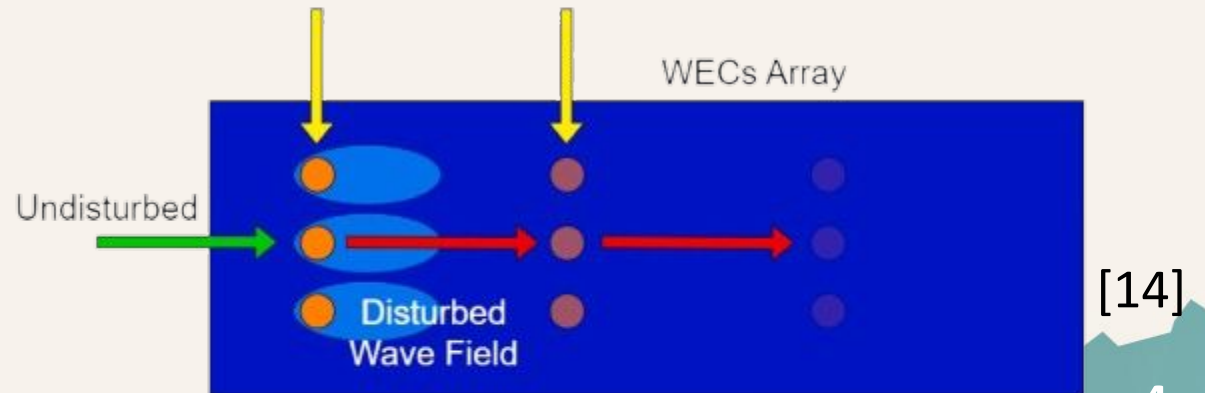
Background → Wave Sheltering

Methods for quantifying this performance rely on **using capture width ratio** to determine how much wave power the device absorbs^{[4-11],[13]}

- This **ignores reflected and dissipated wave energy**, assuming that all energy not absorbed is transmitted

Additionally, WECs are often modeled in isolation, but the end-goal is to deploy WEC arrays

- One study accounted for WEC wakes when considering **array wave sheltering**^[14], but **did not include interactions**, only power available to downstream WECs



Background → Wave Sheltering

Questions:

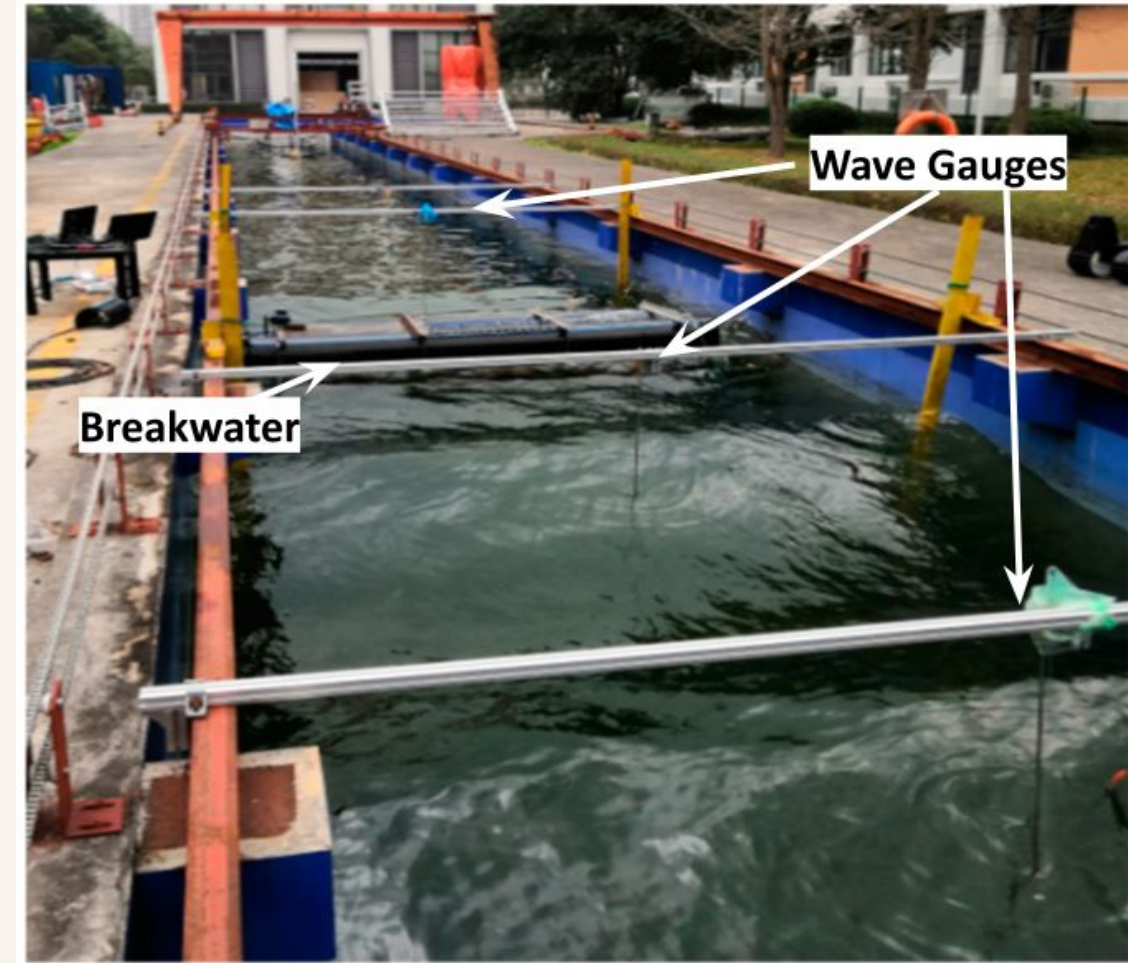
1. How do we define WEC wave sheltering capabilities?
2. How do different WEC architectures perform in this metric?
3. How does this change when including array interactions?



Methodology → Metrics

Standard practice in coastal engineering is to measure wave heights up- and down-stream of a body to determine its dissipative properties^[15]

Some WEC studies have employed this method for a WaveCat^[16] and a point absorber^[17]



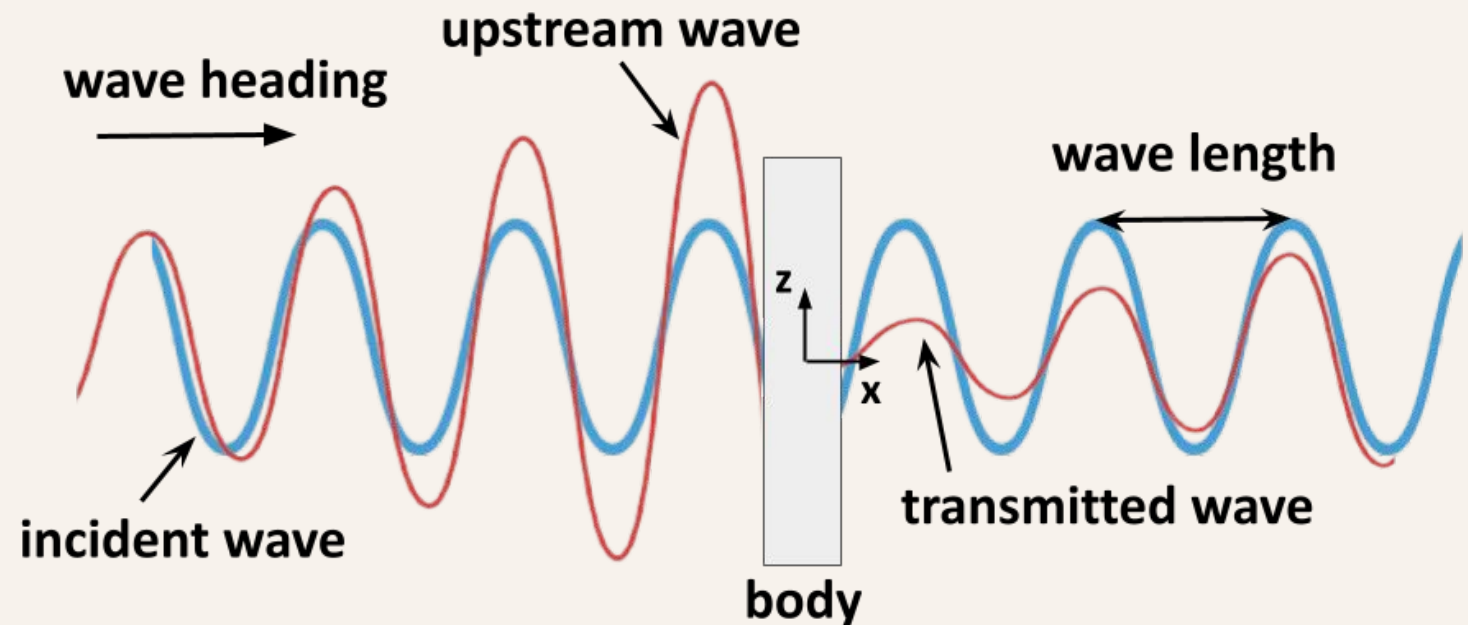
[18]

Methodology → Metrics

We define performance by the transmission (K_t) and reflection (K_r) coefficients^[19]

$$K_t = \frac{|\eta|_{\text{transmitted}}}{|\eta|_{\text{incident}}}$$

$$K_r = \frac{|\eta|_{\text{upstream}}}{|\eta|_{\text{incident}}} - 1$$



η : wave elevation

Methodology → Metrics

The **dissipation coefficient** (K_D) represents **energy that is either dissipated or absorbed** by the WEC and is defined as:

$$K_D = 1 - K_t^2 - K_r^2 \geq 0$$

The **potential power extracted** is defined by Falnes^[20] as:

$$P' = J_{inc} - J_r - J_t \quad [\text{kW/m}]$$

where J is the wave energy transport

$$J = \frac{\rho g}{4\omega} |A|^2$$

ρ : fluid density
 g : gravitational constant
 ω : wave frequency [rad/s]
 A : wave amplitude

Methodology → Metrics

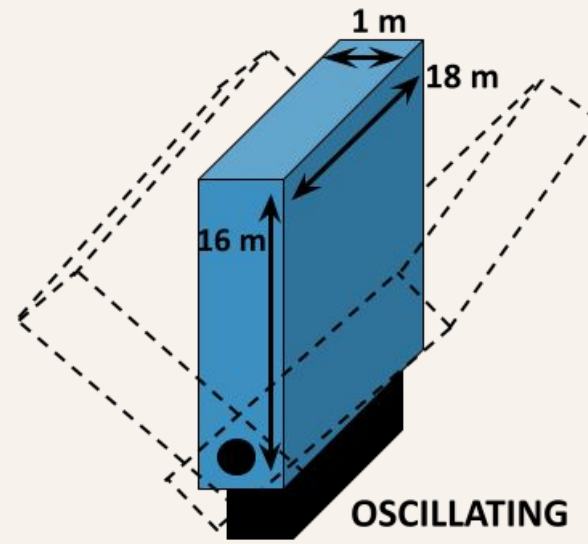
How do we define WEC wave sheltering capabilities?

- K_t and K_r define our device **performance**
- The K_D condition must be met for **energy balance**
- P' is how we define potential **power extracted**

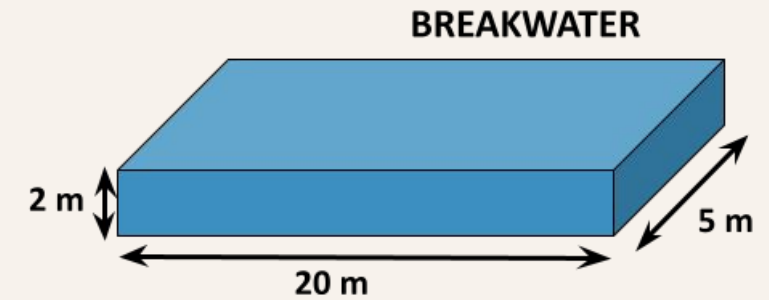
Methodology → Architectures

We analyzed:

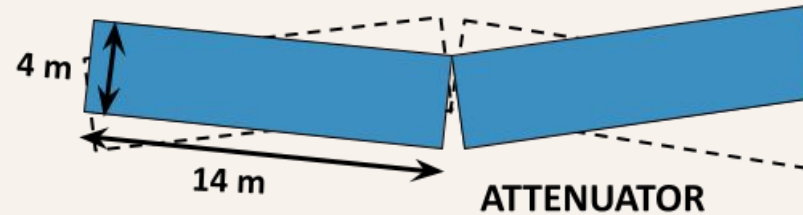
- Oscillating surge (OS)
- Heaving point absorber (PA)
- Attenuator
- Breakwater



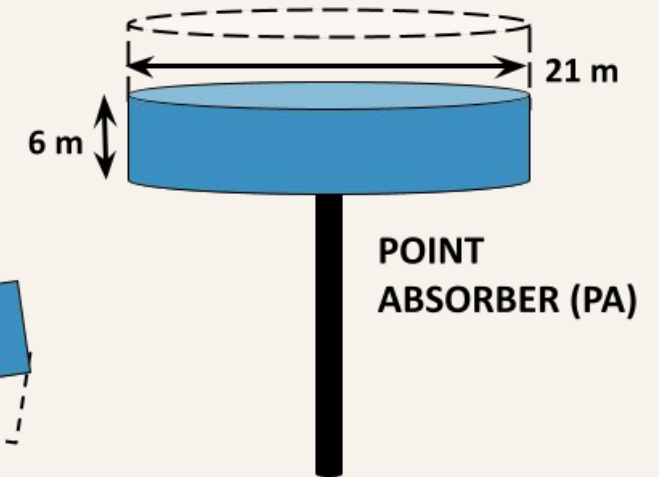
OSCILLATING
SURGE (OS)



BREAKWATER



ATTENUATOR



POINT
ABSORBER (PA)

Individual WECs were sized such that they are **rated for the same power production** (within 5%) at the frequency of interest (1.25 rad/s)

Methodology → Architectures

Each architecture is modeled in **Capytaine**^[21], an open-source boundary element method (BEM) solver

- used to find **hydrodynamic coefficients, incident (η_{inc}), diffracted (η_{diff}), and radiated (η_{rad}) wave elevations**

$$\eta_{tot} = \eta_{inc} + \eta_{diff} + \sum_i X_i \eta_{rad,i} \quad [21]$$

i: degree of freedom
*all values are complex

We still need the complex body motion (X_i) to obtain the correct radiated wave elevation

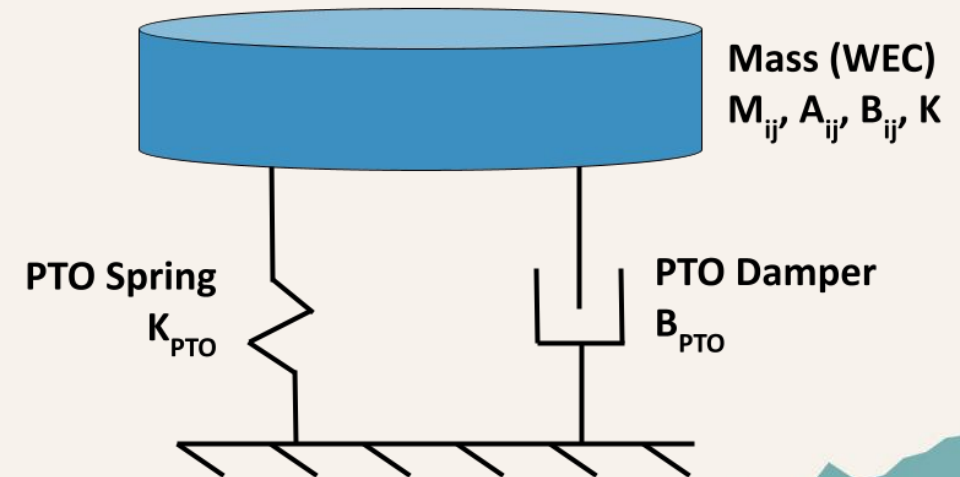
Methodology → Architectures

We use the hydrodynamic coefficients ($M_{ij}, A_{ij}, B_{ij}, K$) to determine body motion

Additionally, we model controllers as **dampers** and as **spring-dampers** (reactive) for each architecture. These will alter body motion (X_i) to resonate with the wave frequency:

$$\frac{X_i}{A} = \frac{F_{ex}}{-\omega^2(M_{ii} + A_{ij}) - i\omega(B_{ij} + B_{PTO}) + K + K_{PTO}}$$

F_{ex} : excitation force
 A : wave amplitude
 X : complex body motion
 $M_{ij}, A_{ij}, B_{ij}, K$: hydro coeffs

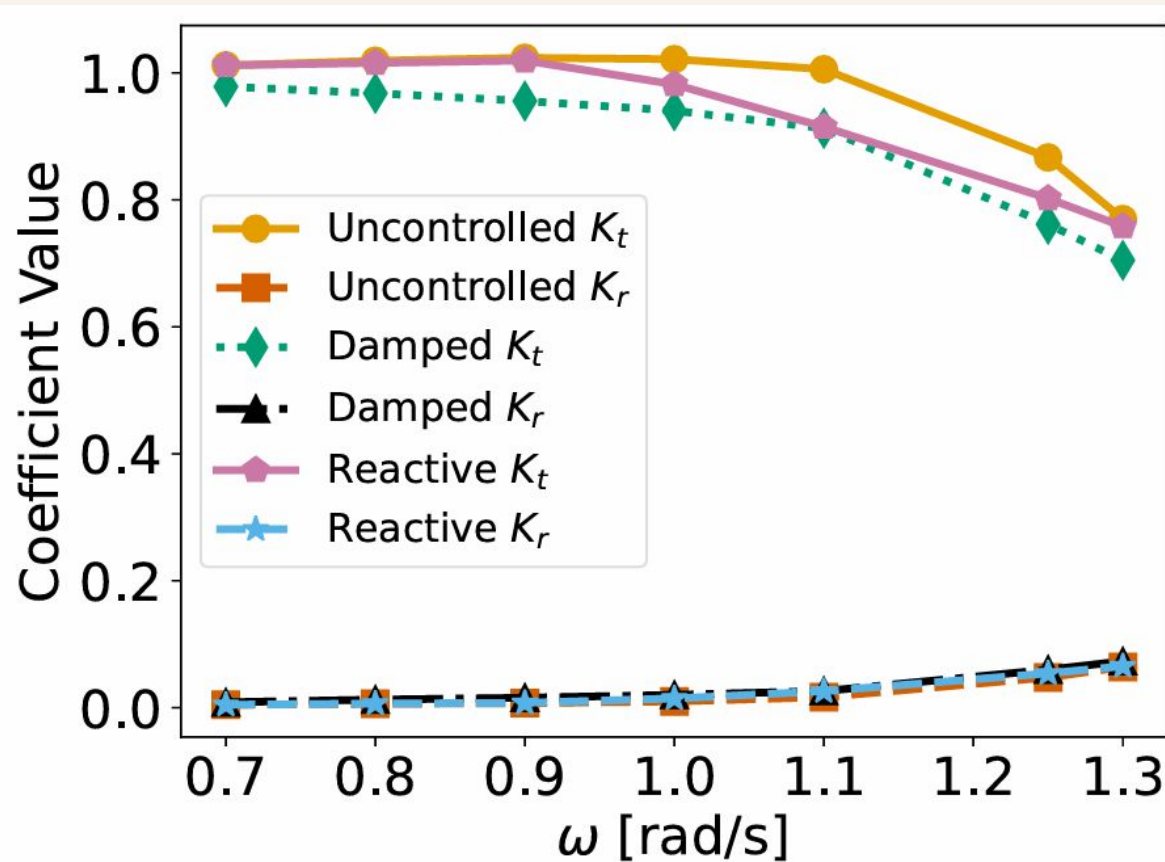


Methodology → Architectures

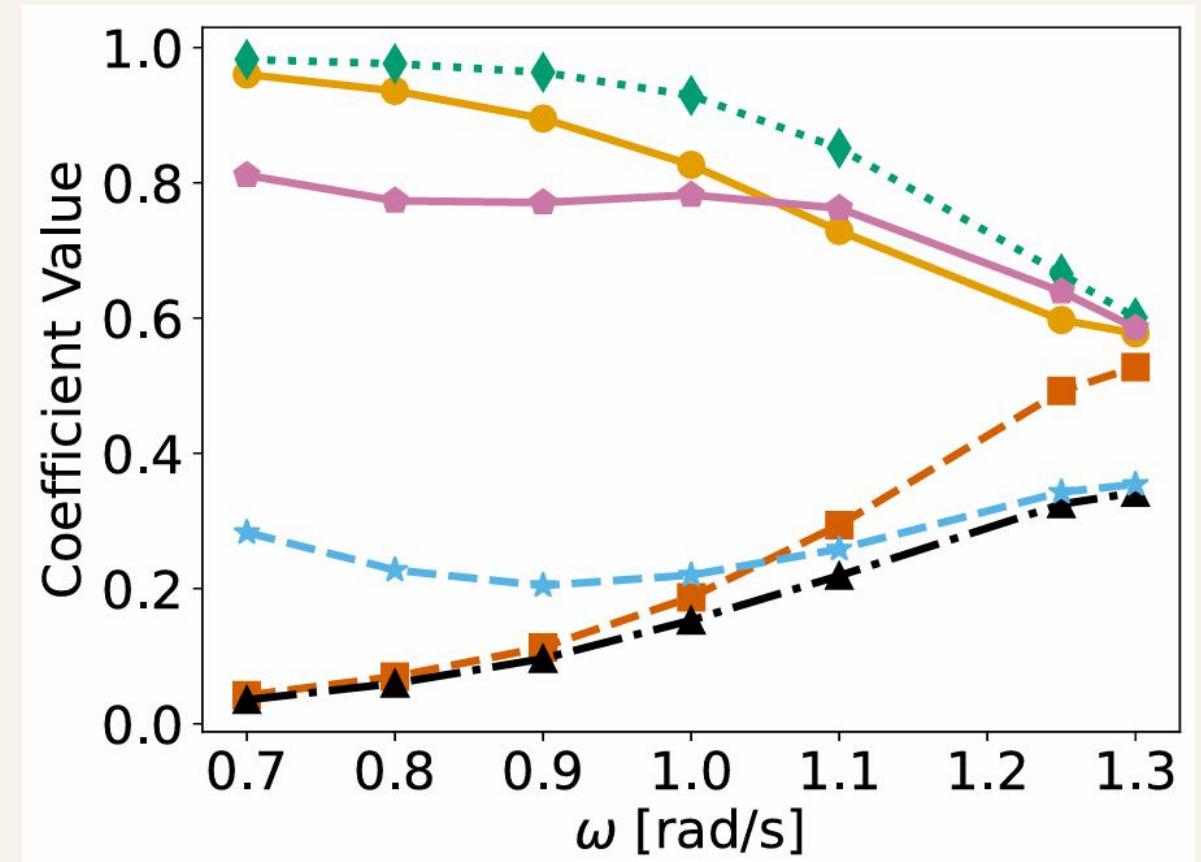
How do different WEC architectures perform in this metric?

- We chose **3 WEC architectures** and 1 breakwater design
- We determine the total **wave elevation**
- We use a **simple control model** and find **complex body motion**

Point Absorber



Oscillating Surge



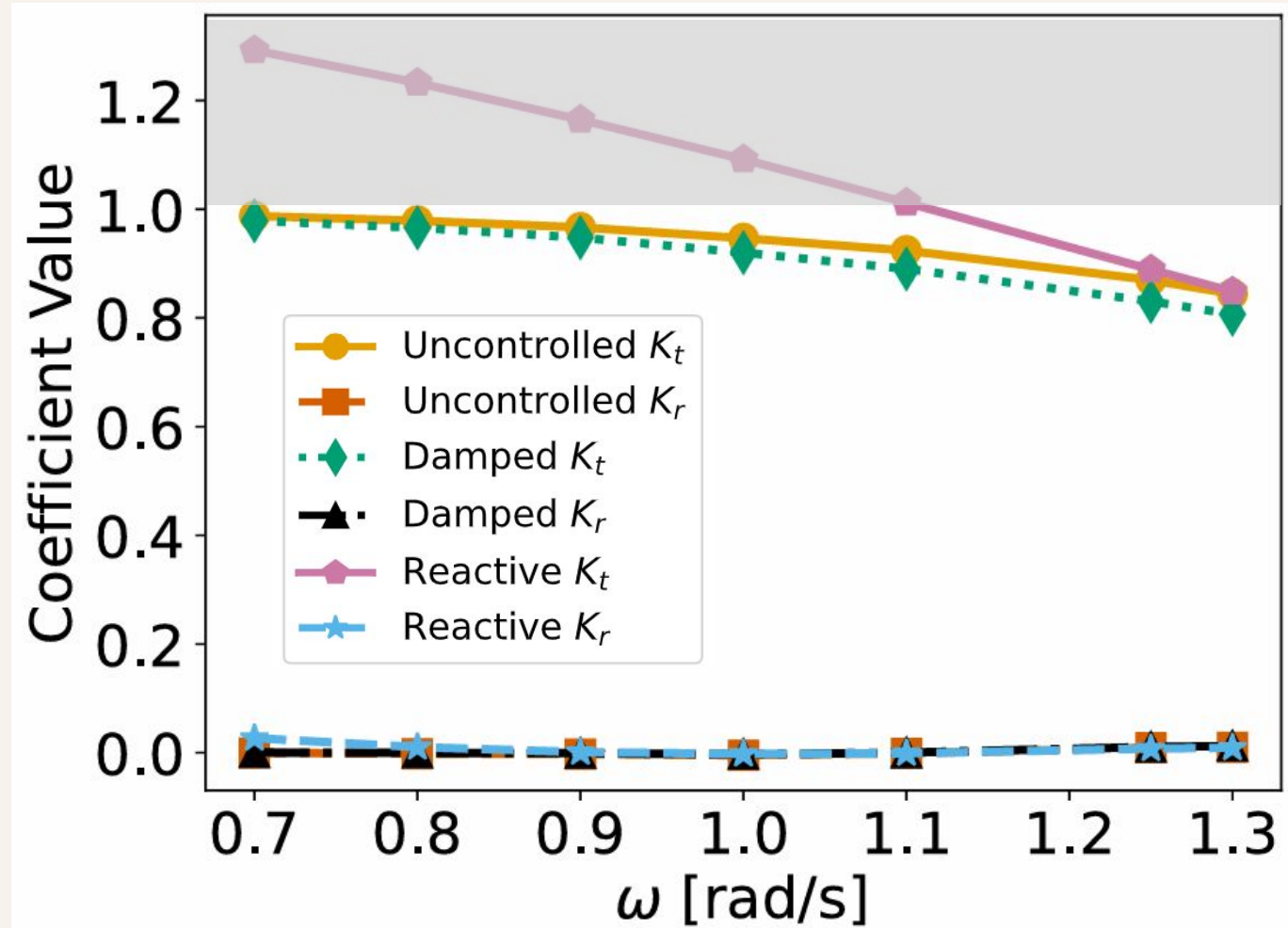
RESULTS →
Single

1. The coefficient **trendline with respect to frequency remains similar** regardless of control scheme
2. Both **perform better at higher frequencies**, with the OSWEC still performing well at low frequencies

Results → Single

The **attenuator violates energy balance** at <1.2 rad/s when **reactively controlled**

- violating linear potential flow assumption of small body amplitude

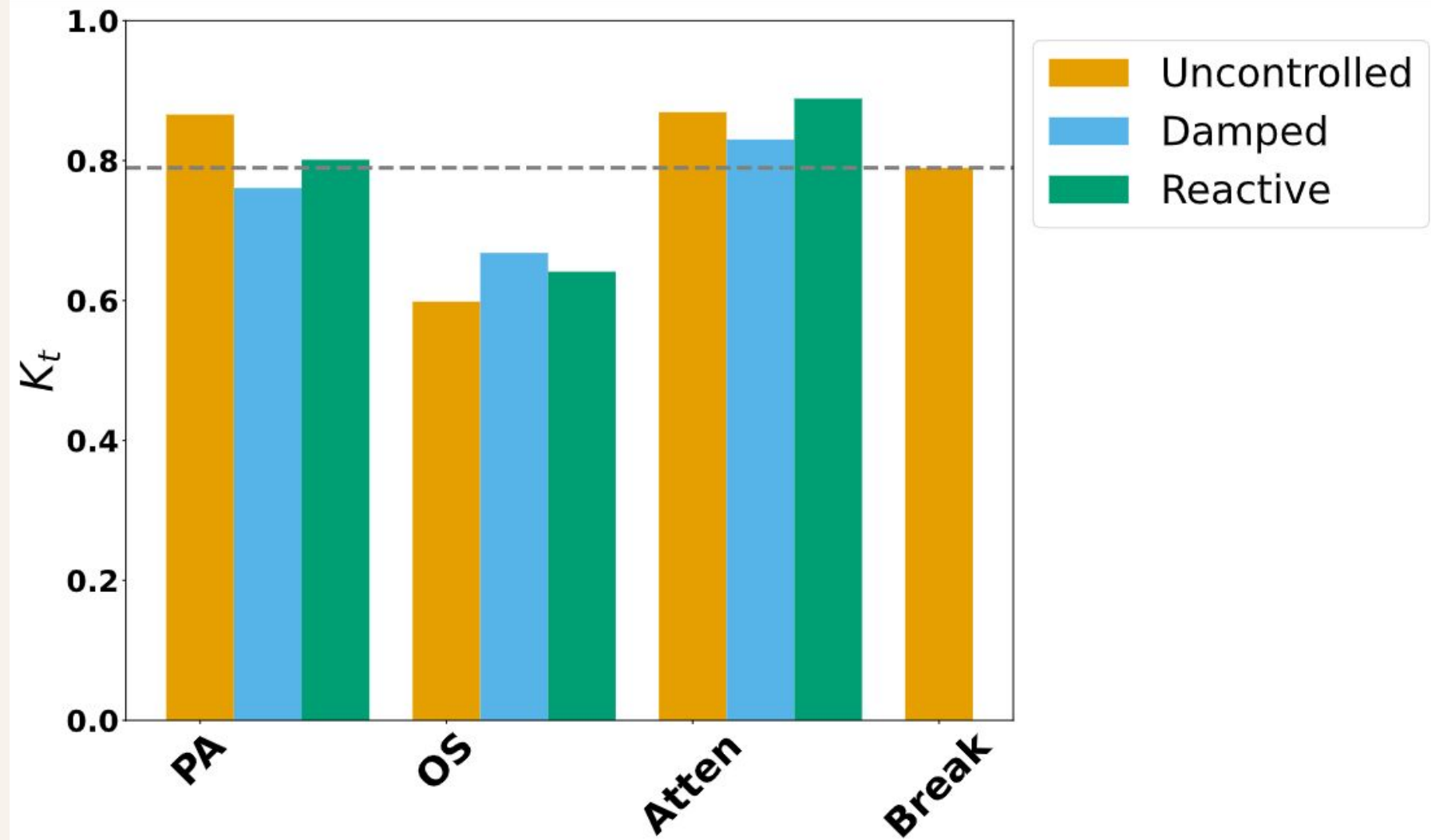


Attenuator

The **OSWEC**
outperforms all other
architectures

The attenuator cannot
outperform the
breakwater

Controls significantly
alter PA and OS
performance (for
better and for worse,
respectively)

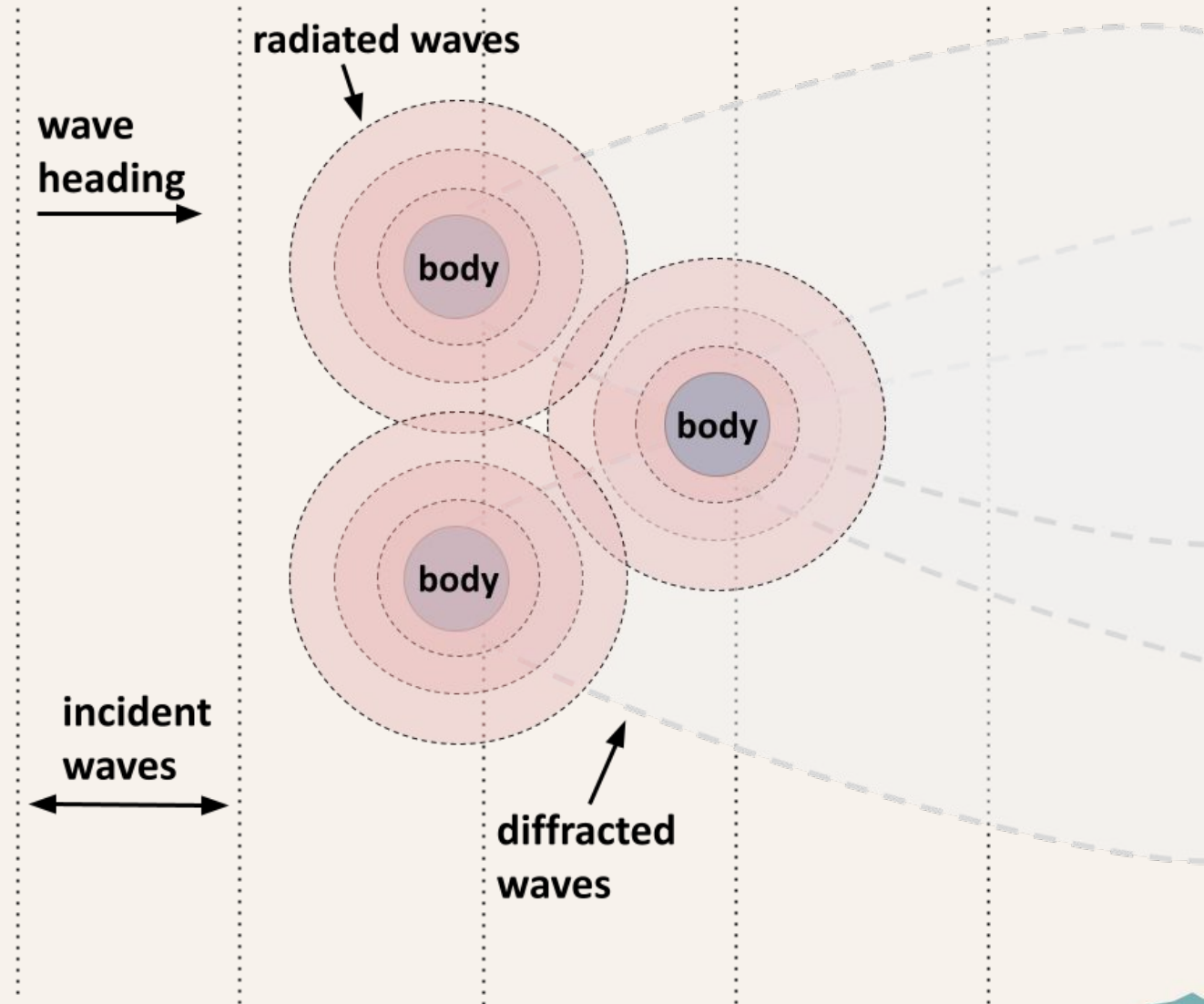


Results → Single

Methodology → Arrays

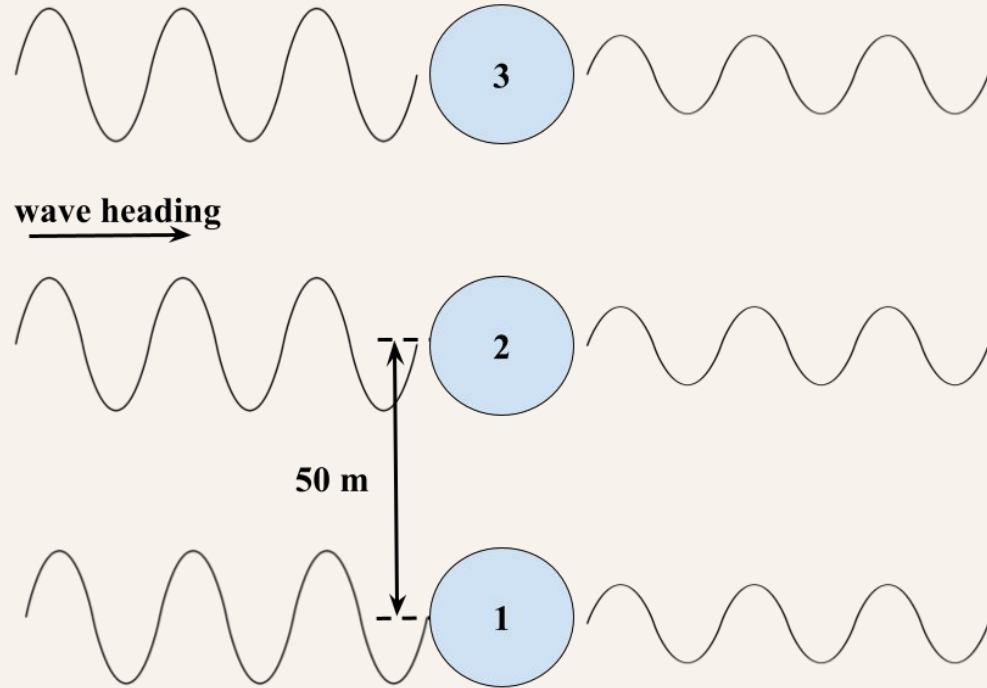
Oscillating bodies can interact in ways that are constructive or destructive to power production^[22,23]

- does this correspond to their wave sheltering performance?

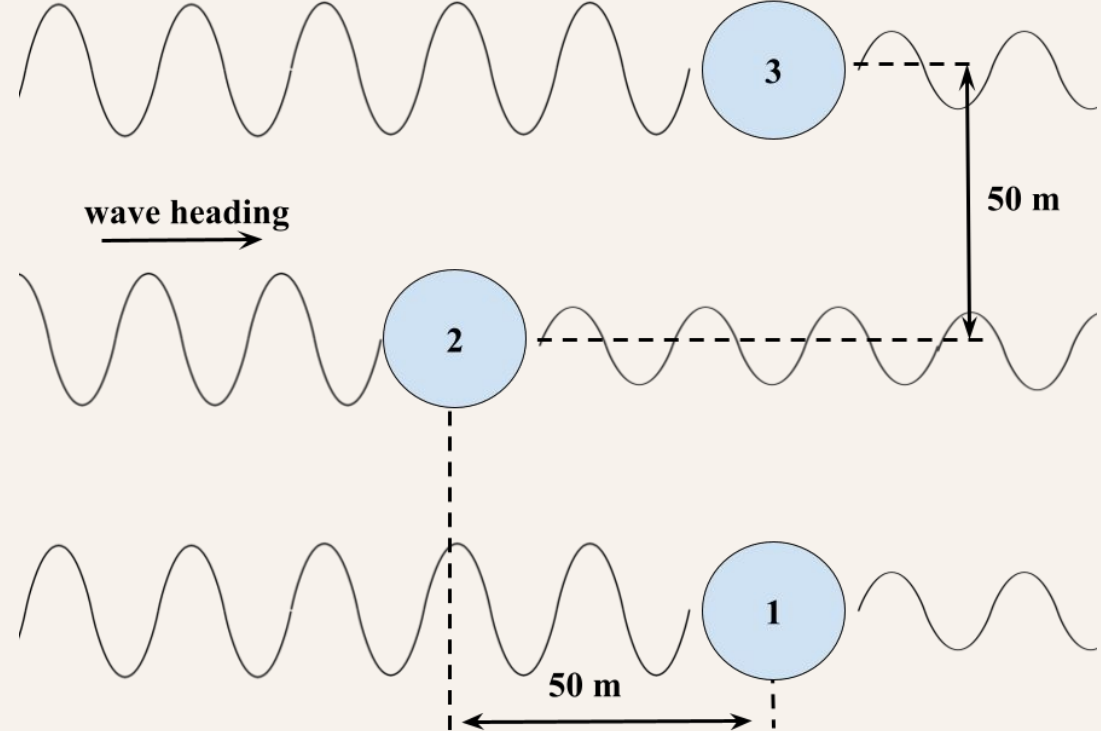


Methodology → Arrays

We model two arbitrary, non-optimized array configurations



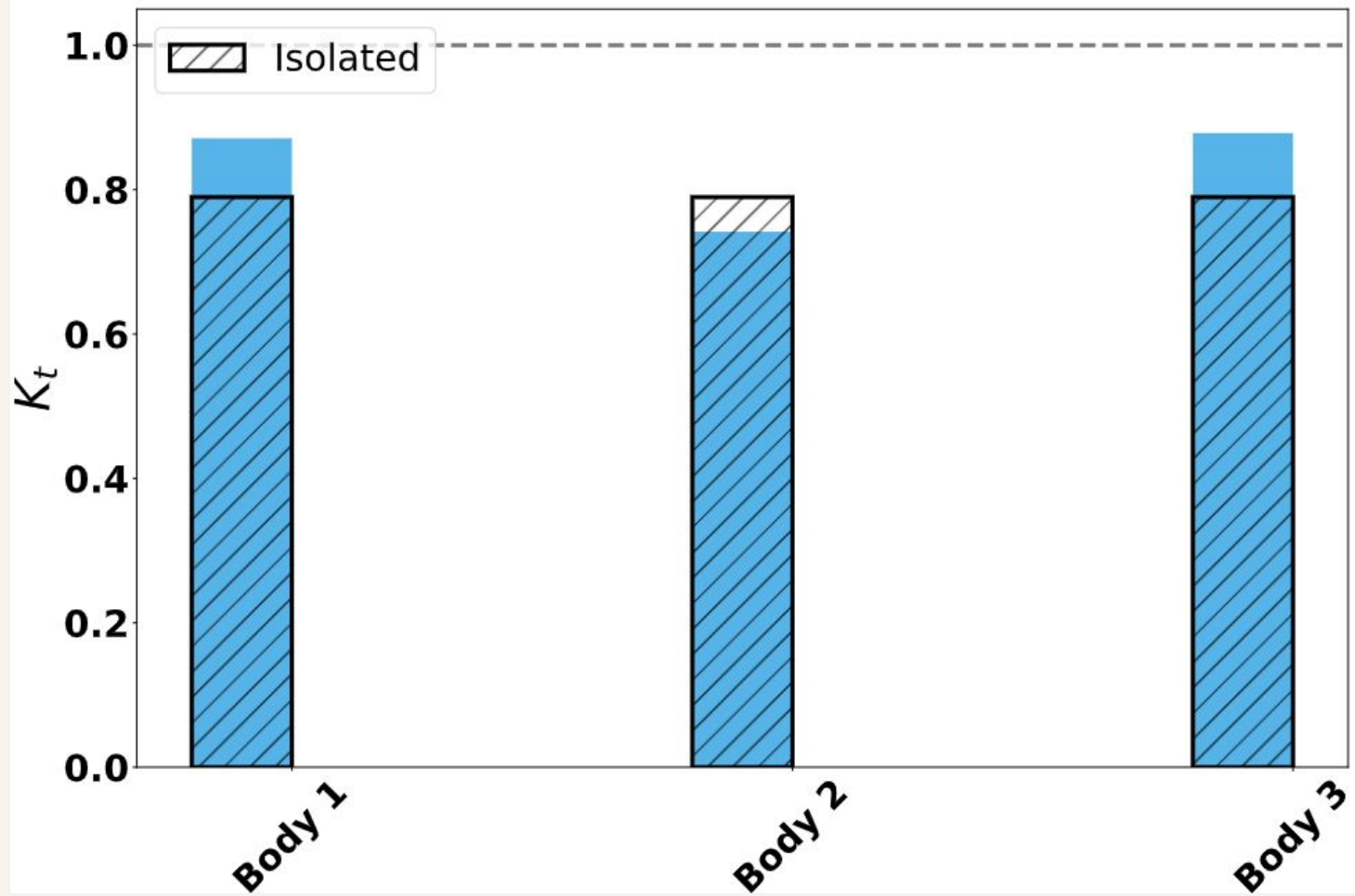
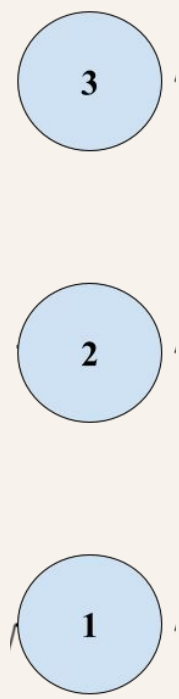
Regular



Staggered

Breakwater

The sheltering effect is **concentrated in the center**, with the periphery experiencing less wave sheltering



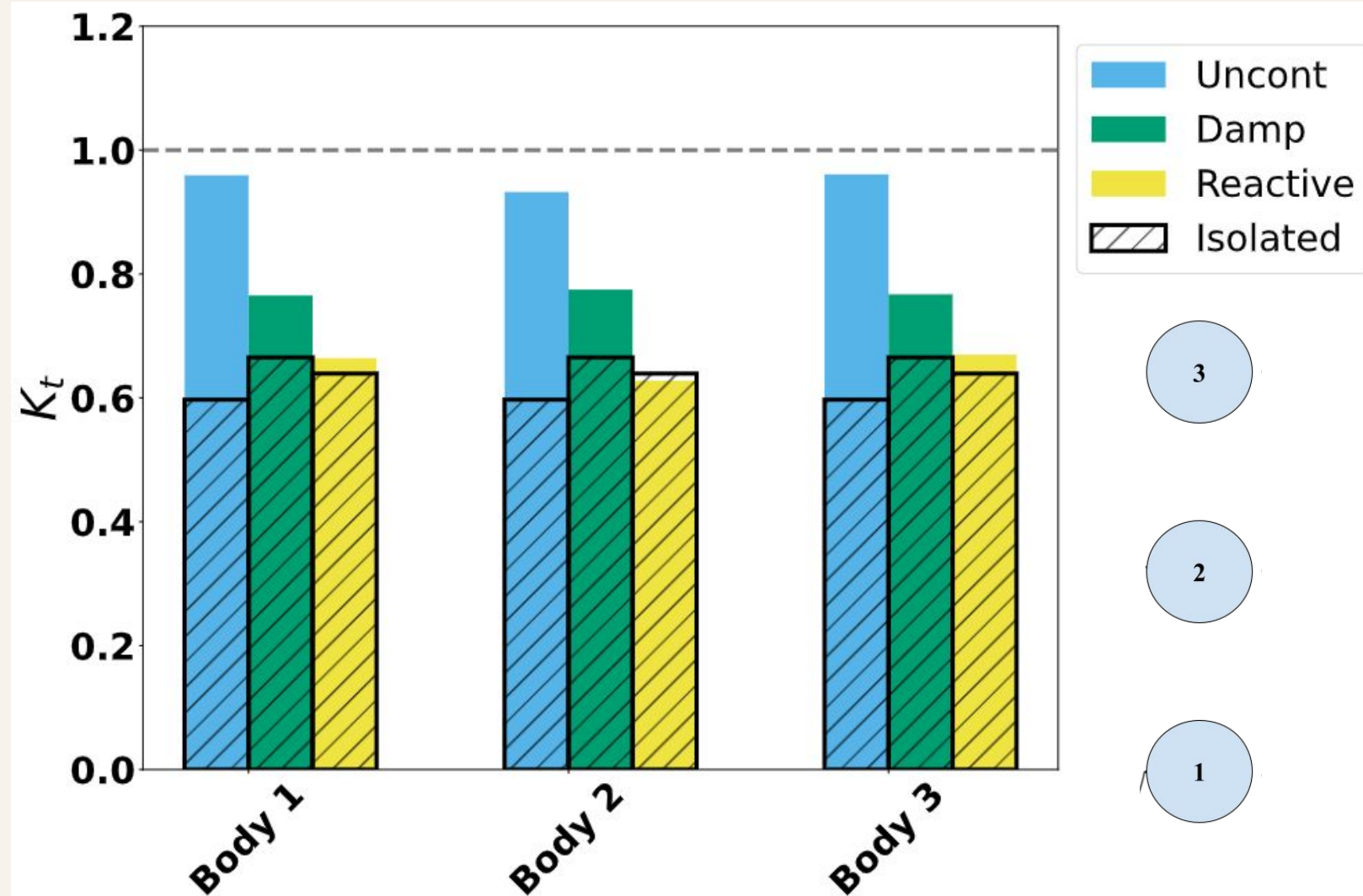
*at a frequency of 1.25 rad/s

Results → Array (Regular)

Results → Array (Regular) OSWEC

We see modeling the body in isolation is **underpredicting wave transmission** for the uncontrolled and damped cases

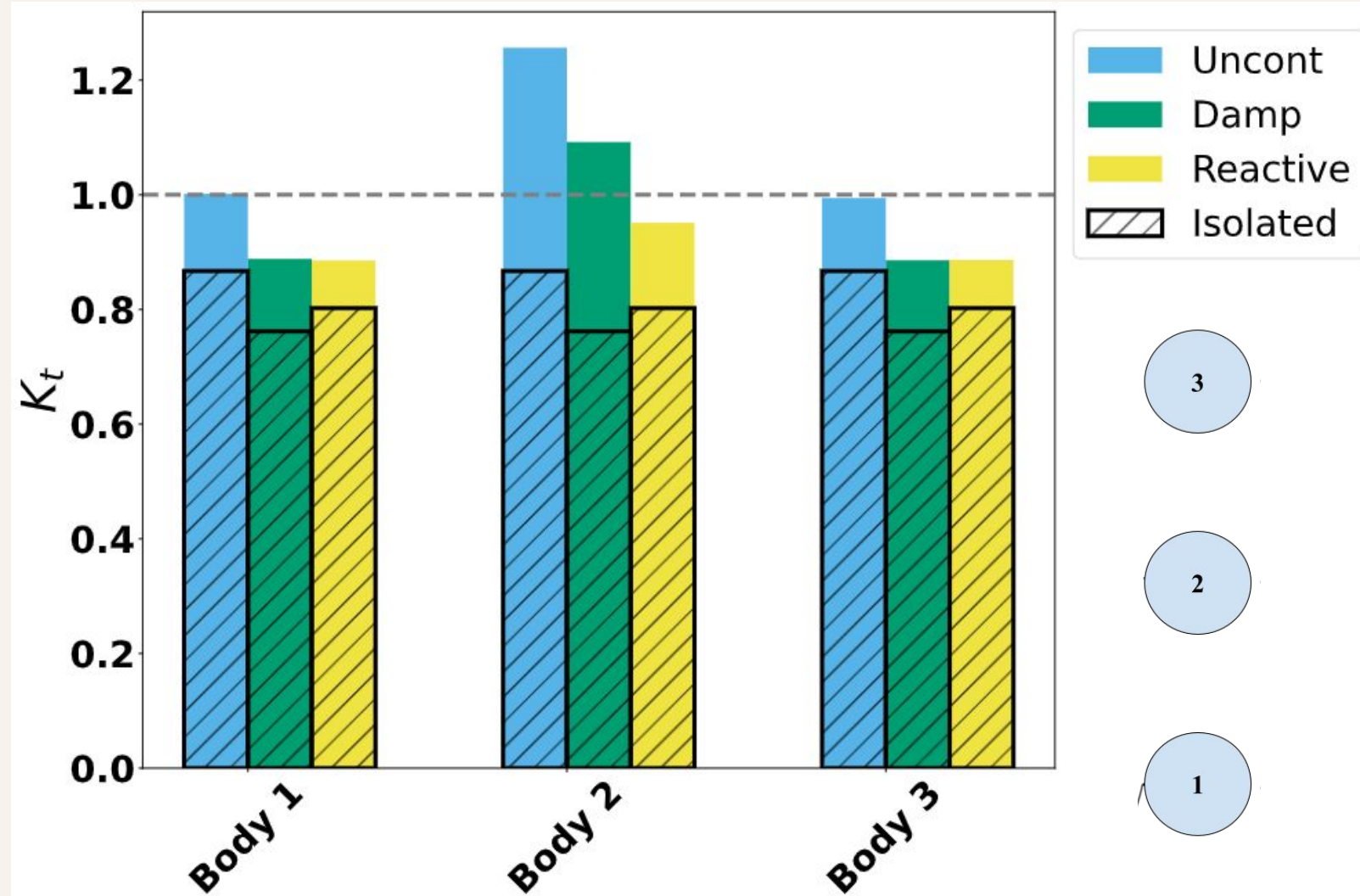
There is **little change** when the bodies are reactively controlled



*at a frequency of 1.25 rad/s

Results → Array (Regular) Point Absorber

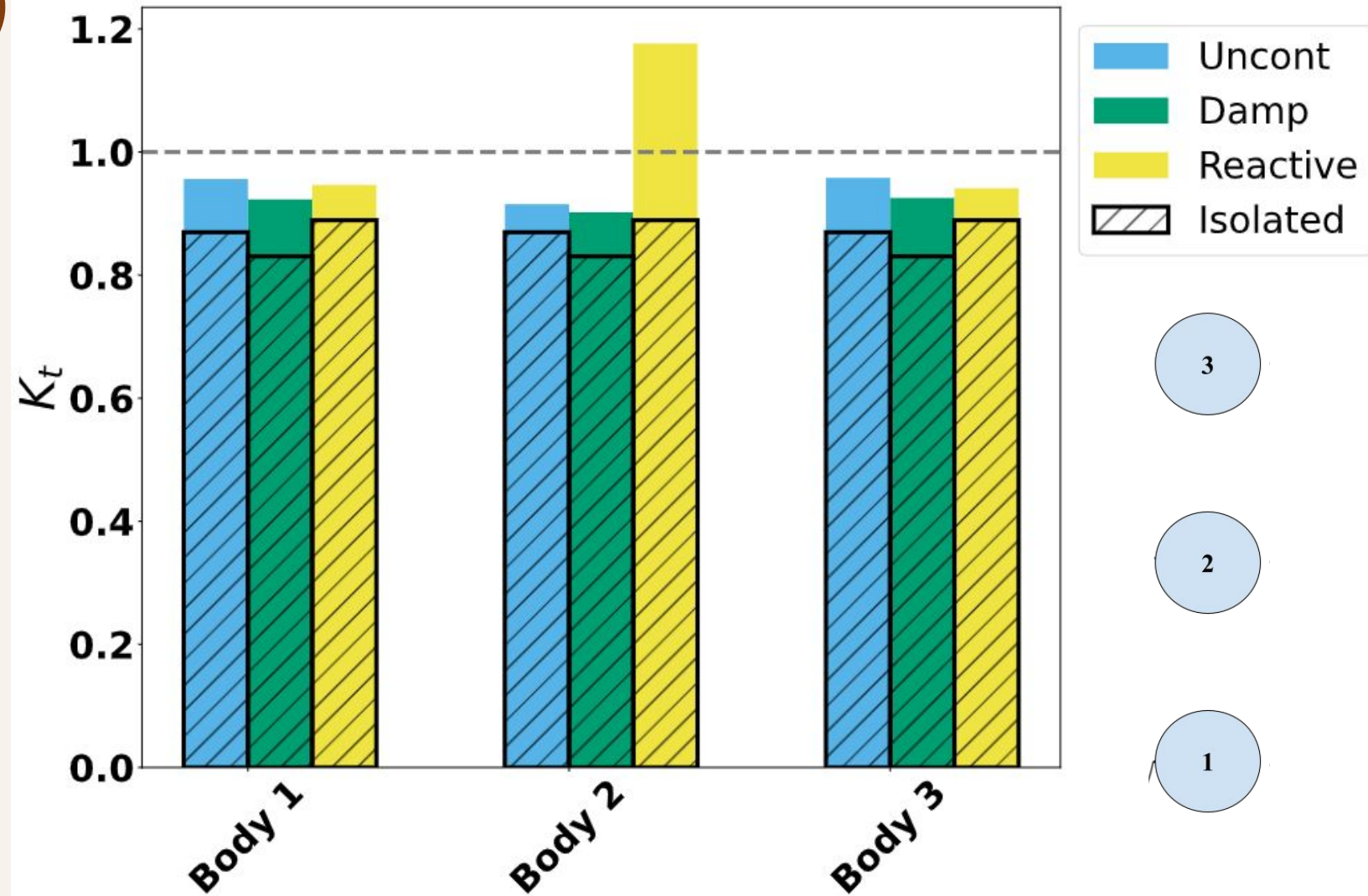
We see the **wave sheltering of Body 2** negated by interactions of Bodies 1 and 3 in the damped control case.



*at a frequency of 1.25 rad/s

Results → Array (Regular) Attenuator

We see a **slight underprediction** and again energy balance violation with reactive control



*at a frequency of 1.25 rad/s

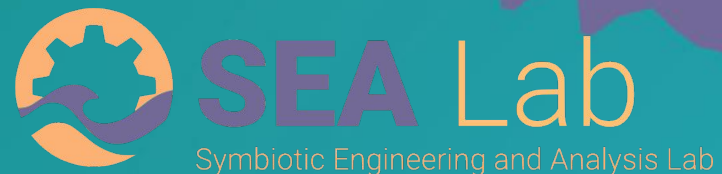
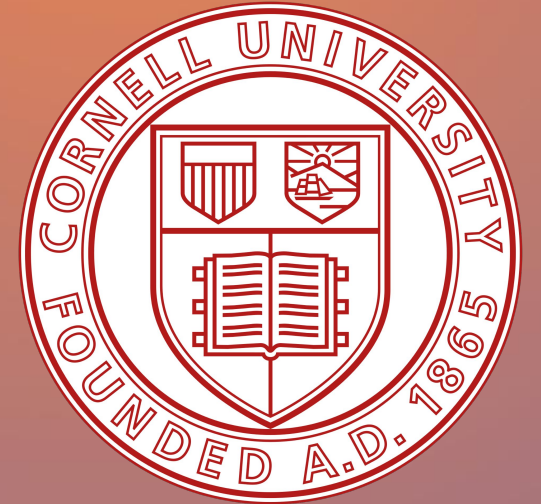
Conclusions

1. We defined WEC **wave sheltering capabilities by their fluid-structure interactions** (K_t and K_r)
2. We determined the **OSWEC architecture** had the lowest wave transmission across frequencies and the **breakwater typically outperforms the PA and attenuator**
3. We saw that wave sheltering performance can be **affected by array interactions**, but the extent to which this is relevant in the far field needs further investigation

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Thank You! Questions?

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GitHub (to be released):
<https://github.com/symbiotic-engineering/transmission-reflection>

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