



# Sheltering effect of various wave energy converter archetypes in arrays

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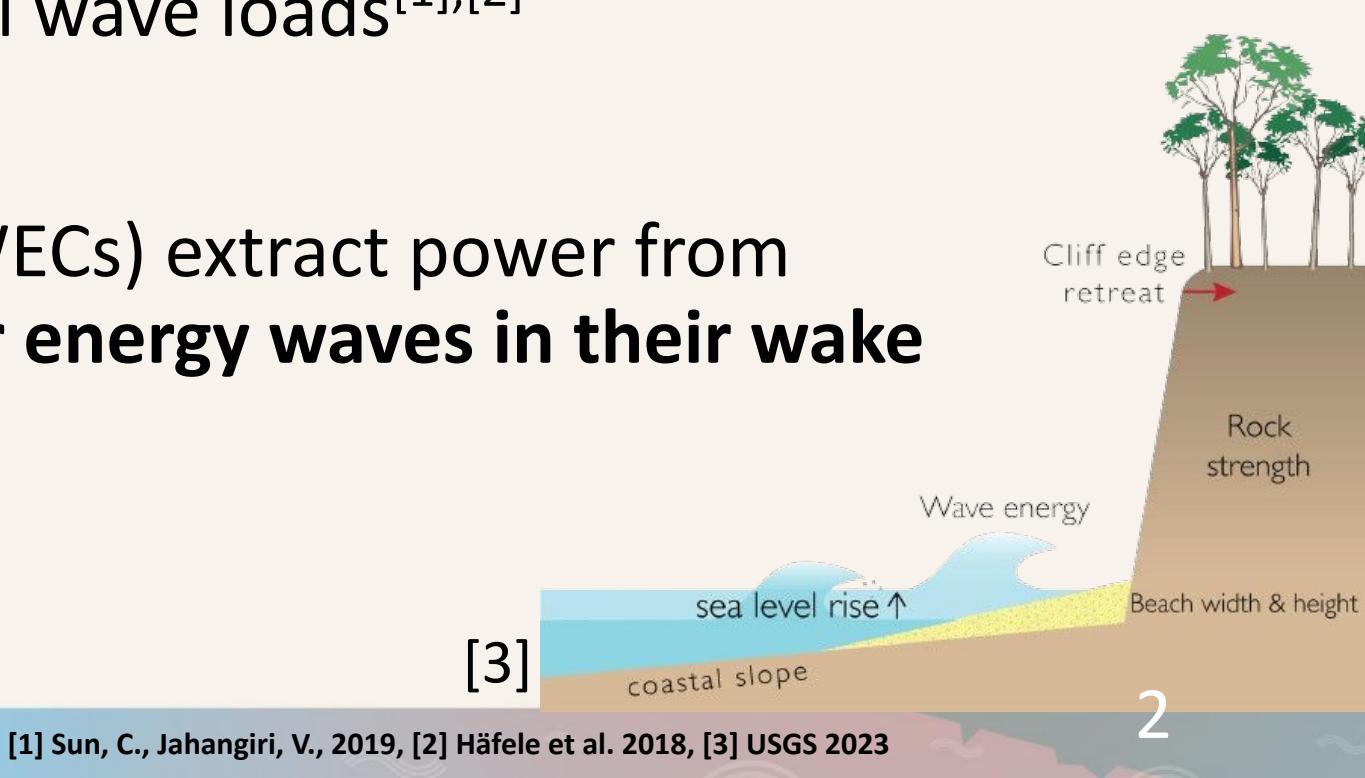
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Symbiotic Engineering and Analysis Lab



# Background → Wave Sheltering

Offshore structures and coastlines face **fatigue damage and deterioration** due to cyclical wave loads<sup>[1],[2]</sup>

Wave energy converters (WECs) extract power from ocean waves, leaving **lower energy waves in their wake**

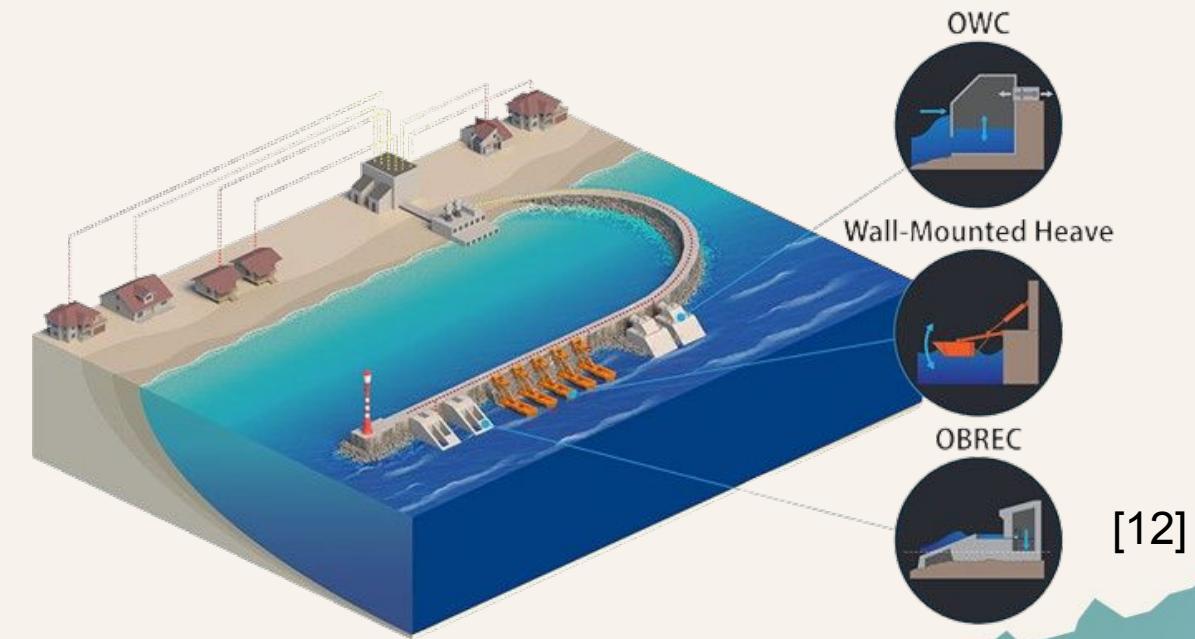


# Background → Wave Sheltering

Studies have investigated the **wave sheltering capabilities of different WECs** for protecting vulnerable coastlines<sup>[4],[5],[6],[7]</sup>, offshore aquaculture farms<sup>[8]</sup>, and offshore wind installations<sup>[9],[10],[11]</sup>

NREL<sup>[12]</sup> is working to construct **coastal structure integrated WECs**, which are attached to traditional fixed breakwaters

This presentation focuses specifically on **floating WECs**



[12]

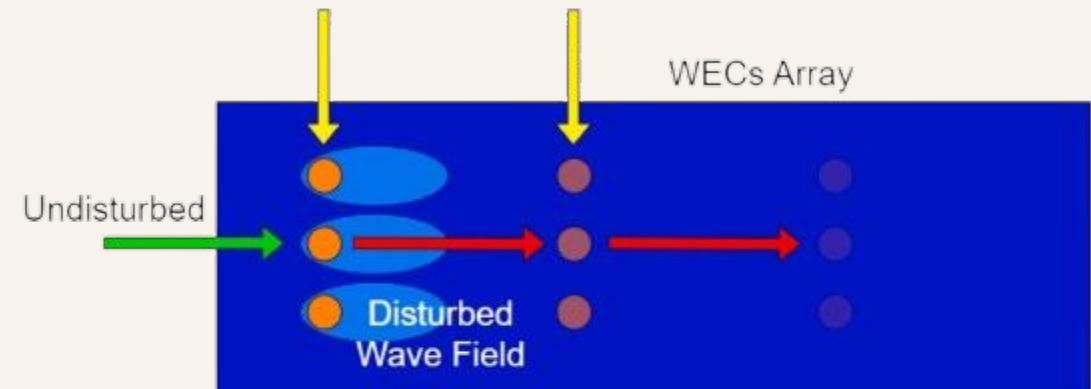
# Background → Wave Sheltering

Methods for quantifying this performance rely on **using capture width ratio** to determine how much wave power the device absorbs<sup>[4-11],[13]</sup>

- This **ignores reflected and dissipated wave energy**, assuming that all energy not absorbed is transmitted

Additionally, WECs are often modeled in isolation, but the end-goal is to deploy WEC arrays

- One study accounted for WEC wakes when considering **array wave sheltering<sup>[14]</sup>**, **but did not include interactions**, only power available to downstream WECs



[14]

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# Background → Wave Sheltering

## Questions:

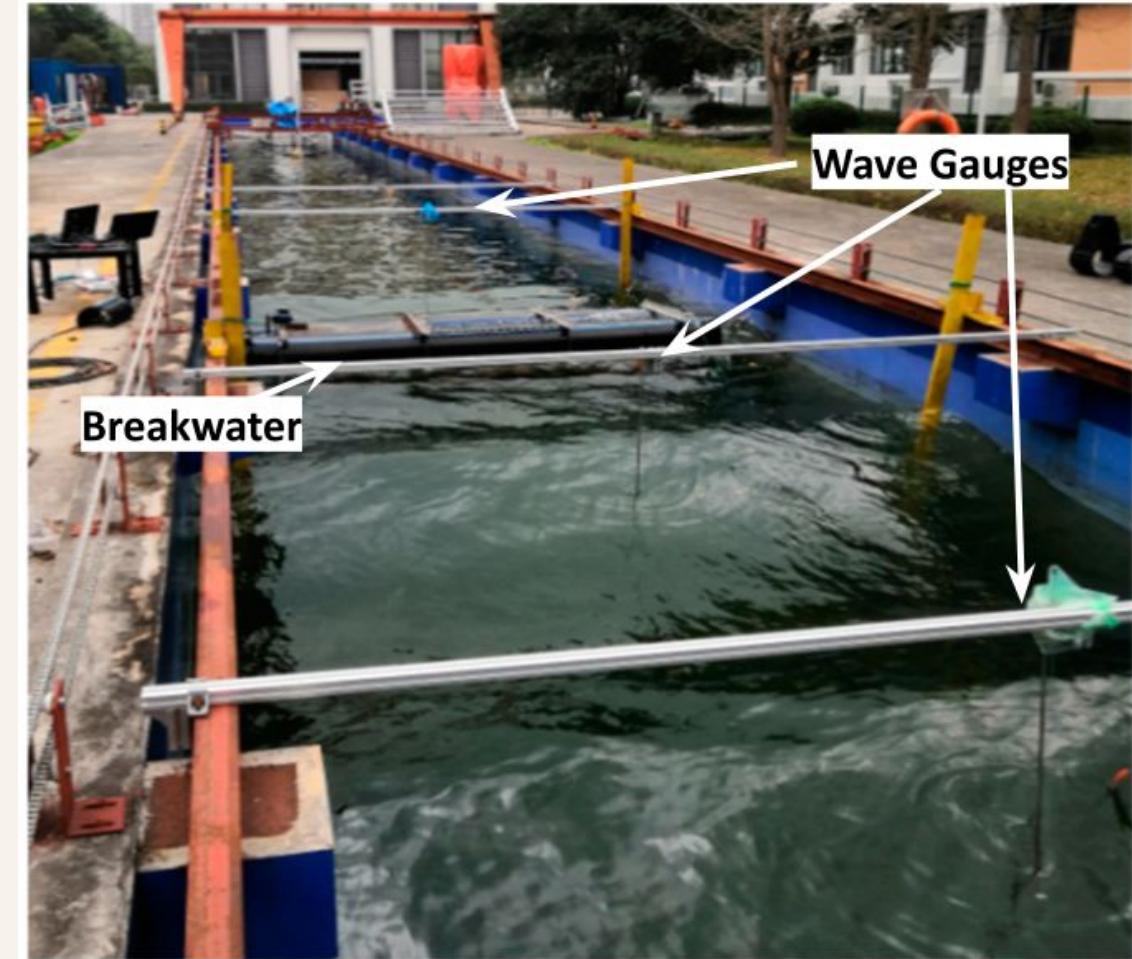
1. How do we define WEC wave sheltering capabilities?
2. How do different WEC architectures perform in this metric?
3. How does this change when including array interactions?



# Methodology → Metrics

Standard practice in coastal engineering is to measure wave heights up- and down-stream of a body to determine its dissipative properties<sup>[15]</sup>

Some WEC studies have employed this method for a WaveCat<sup>[16]</sup> and a point absorber<sup>[17]</sup>



[18]

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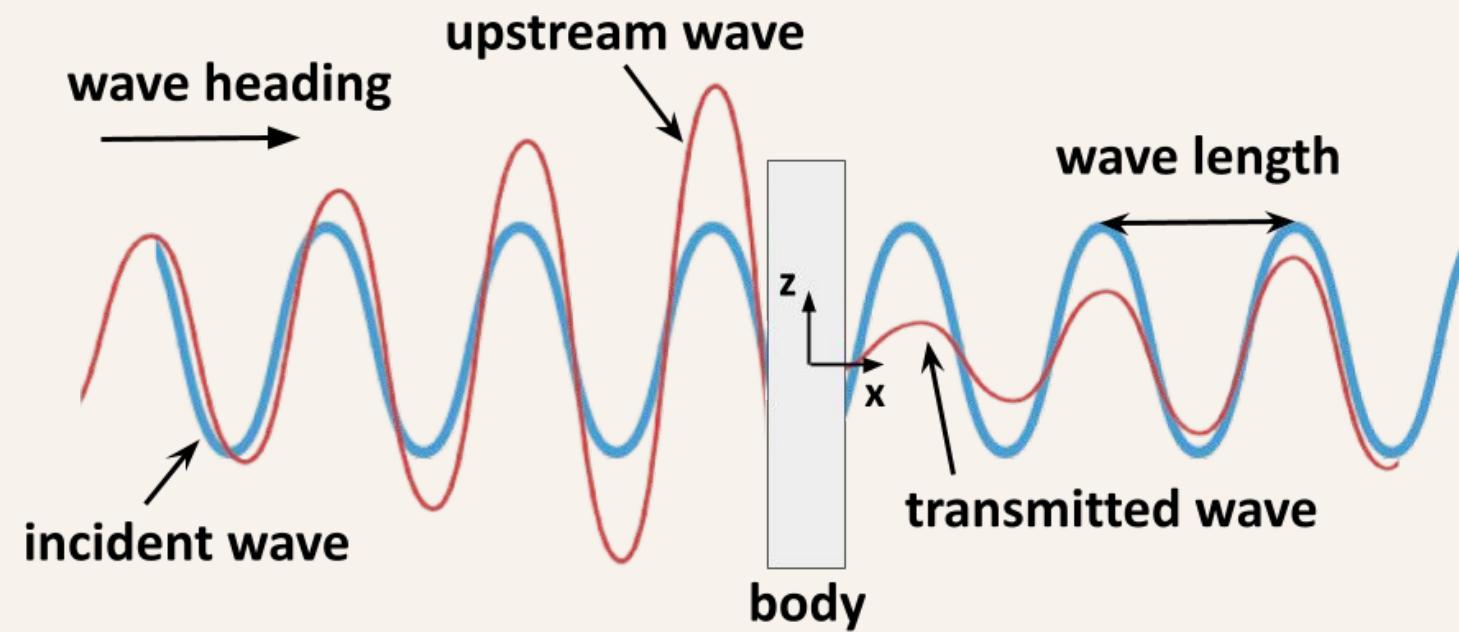
[15] Seelig 1980, [16] Carballo, Iglesias, 2013, [17] Atan et al. 2019, [18] Bao et al. 2022.

# Methodology → Metrics

We define performance by the transmission ( $K_t$ ) and reflection ( $K_r$ ) coefficients<sup>[19]</sup>

$$K_t = \frac{|\eta|_{\text{transmitted}}}{|\eta|_{\text{incident}}}$$

$$K_r = \frac{|\eta|_{\text{upstream}}}{|\eta|_{\text{incident}}} - 1$$



η: wave elevation

# Methodology → Metrics

The **dissipation coefficient ( $K_D$ )** represents **energy that is either dissipated or absorbed** by the WEC and is defined as:

$$K_D = 1 - K_t^2 - K_r^2 \geq 0$$

The **potential power extracted** is defined by Falnes<sup>[20]</sup> as:

$$P' = J_{\text{inc}} - J_r - J_t \quad [\text{kW/m}]$$

where  $J$  is the wave energy transport

$$J = \frac{\rho g}{4\omega} |A|^2$$

$\rho$ : fluid density  
 $g$ : gravitational constant  
 $\omega$ : wave frequency [rad/s]  
 $A$ : wave amplitude

# Methodology → Metrics

How do we define WEC wave sheltering capabilities?

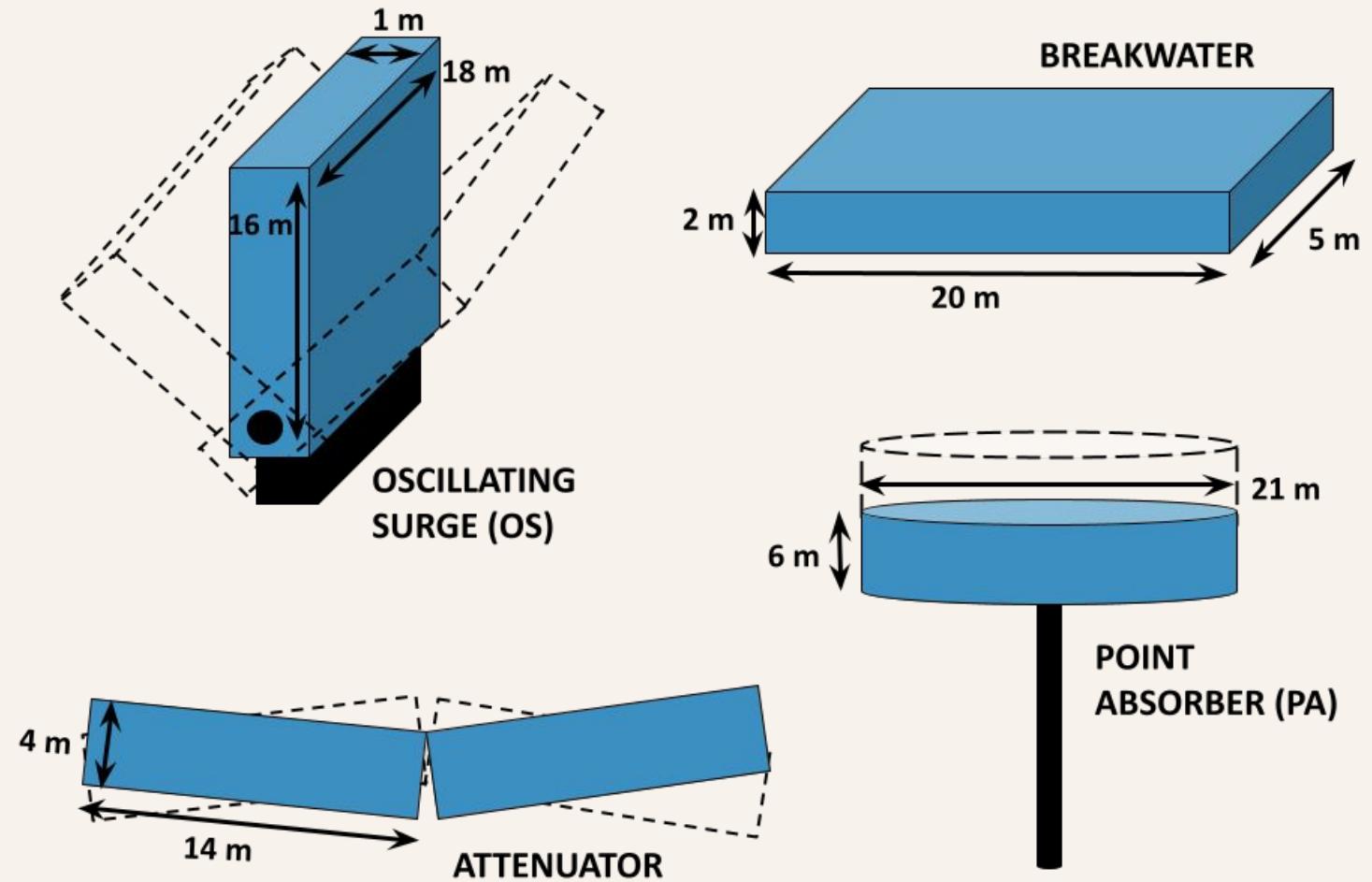
- $K_t$  and  $K_r$  define our device **performance**
- The  $K_D$  condition must be met for **energy balance**
- $P'$  is how we define potential **power extracted**



# Methodology → Architectures

We analyzed:

- Oscillating surge (OS)
- Heaving point absorber (PA)
- Attenuator
- Breakwater



Individual WECs were sized such that they are **rated for the same power production** (within 5%) at the frequency of interest (1.25 rad/s)

# Methodology → Architectures

Each architecture is modeled in **Capytaine**<sup>[21]</sup>, an open-source boundary element method (BEM) solver

- used to find **hydrodynamic coefficients, incident ( $\eta_{\text{inc}}$ ), diffracted ( $\eta_{\text{diff}}$ ), and radiated ( $\eta_{\text{rad}}$ ) wave elevations**

$$\eta_{\text{tot}} = \eta_{\text{inc}} + \eta_{\text{diff}} + \sum X_i \eta_{\text{rad},i}$$

<sup>[21]</sup>  
i: degree of freedom  
\*all values are complex

We still need the complex body motion ( $X_i$ ) to obtain the correct radiated wave elevation

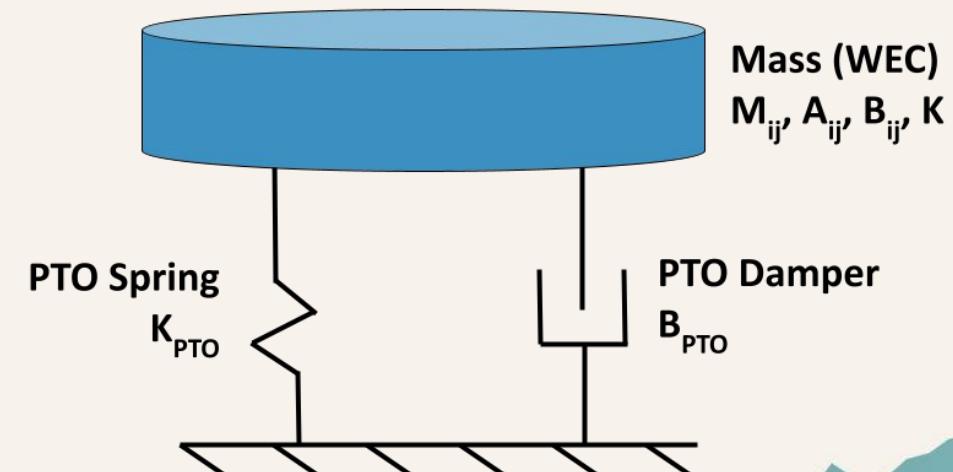
# Methodology → Architectures

We use the hydrodynamic coefficients ( $M_{ij}, A_{ij}, B_{ij}, K$ ) to determine body motion

Additionally, we model controllers as **dampers** and as **spring-dampers** (reactive) for each architecture. These will alter body motion ( $X_i$ ) to resonate with the wave frequency:

$$\frac{X_i}{A} = \frac{F_{ex}}{-\omega^2(M_{ii} + A_{ij}) - i\omega(B_{ij} + B_{PTO}) + K + K_{PTO}}$$

$F_{ex}$ : excitation force  
A: wave amplitude  
X: complex body motion  
 $M_{ii}, A_{ij}, B_{ij}, K$ : hydro coeffs



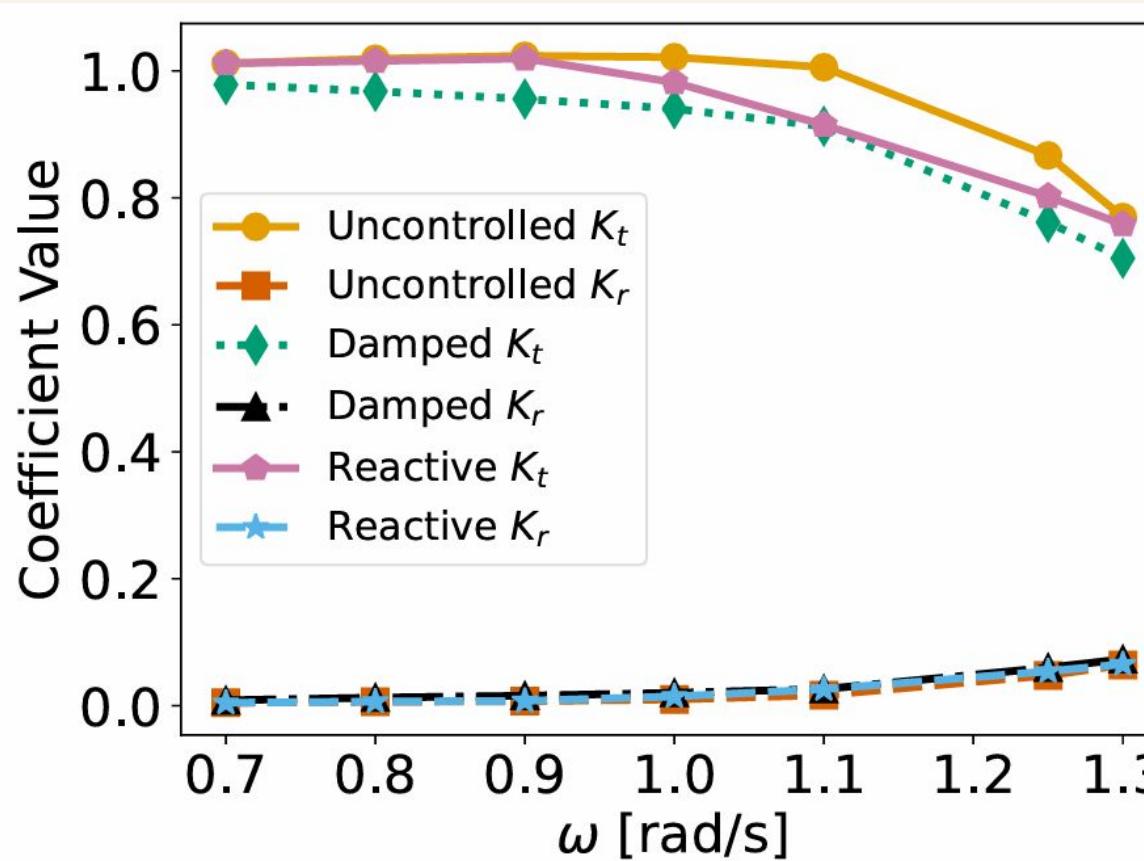
# Methodology → Architectures

How do different WEC architectures perform in this metric?

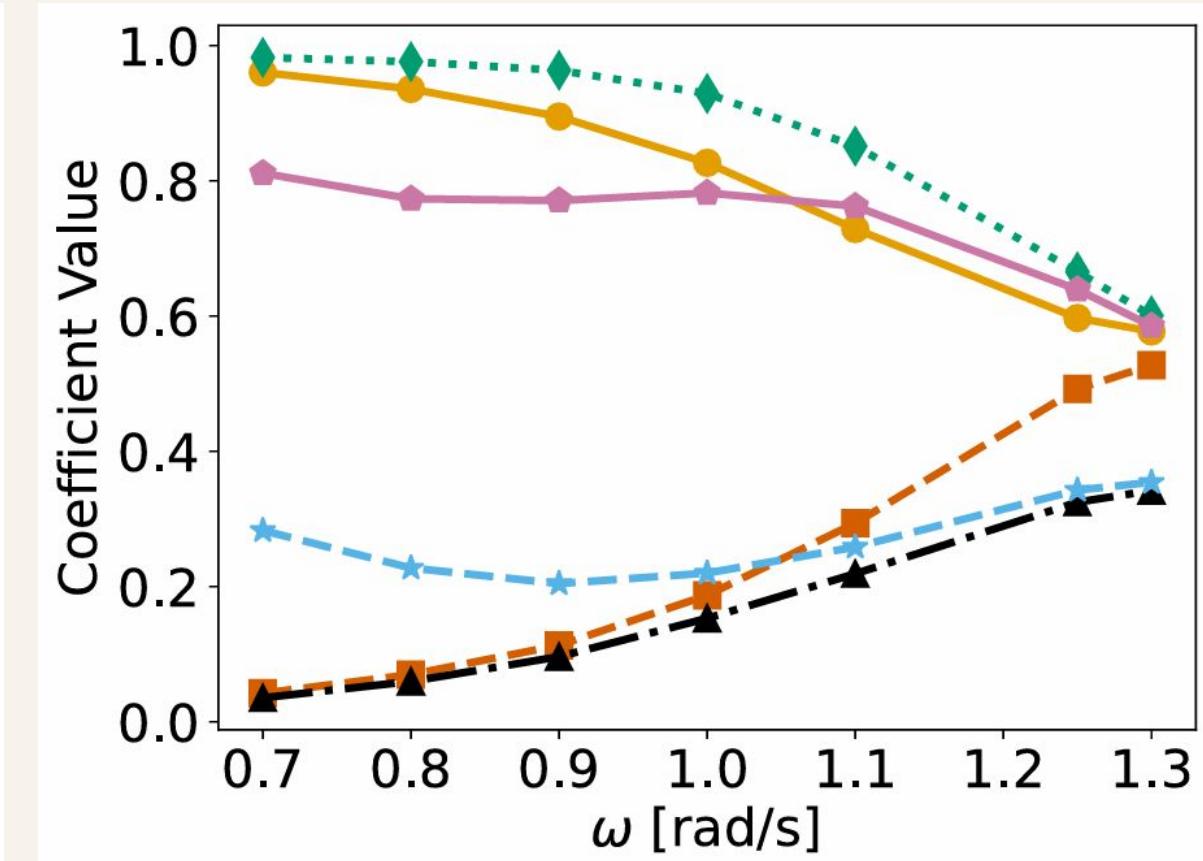
- We chose **3 WEC architectures** and 1 breakwater design
- We determine the total **wave elevation**
- We use a **simple control model** and find **complex body motion**



## Point Absorber



## Oscillating Surge



RESULTS →

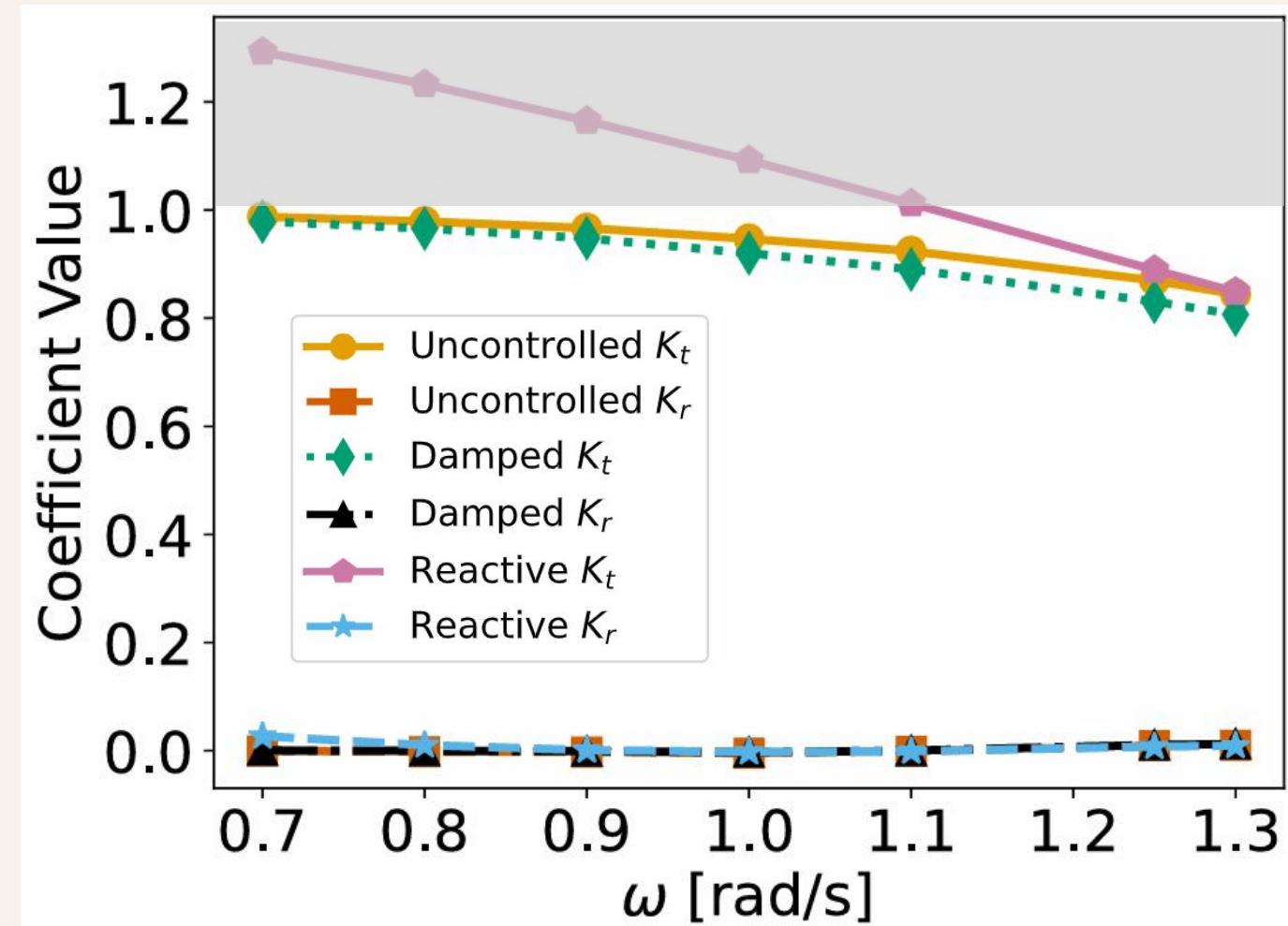
Single

1. The coefficient **trendline with respect to frequency** remains similar regardless of control scheme
2. Both **perform better at higher frequencies**, with the OSWEC still performing well at low frequencies

# Results → Single

The **attenuator violates energy balance** at  $<1.2$  rad/s when **reactively controlled**

- violating linear potential flow assumption of small body amplitude



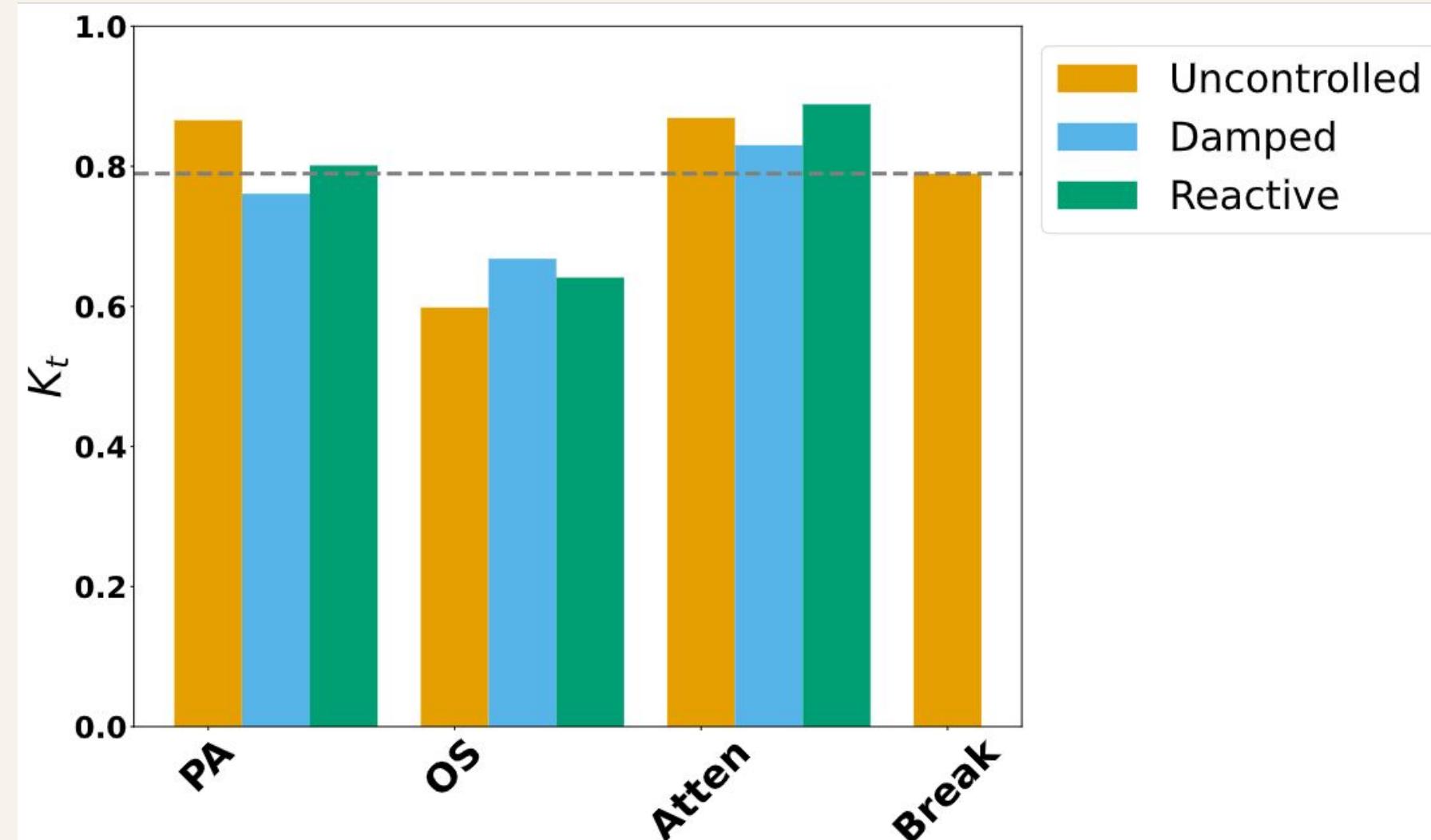
Attenuator

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The **OSWEC** outperforms all other architectures

The attenuator cannot outperform the breakwater

Controls significantly alter PA and OS performance (for better and for worse, respectively)

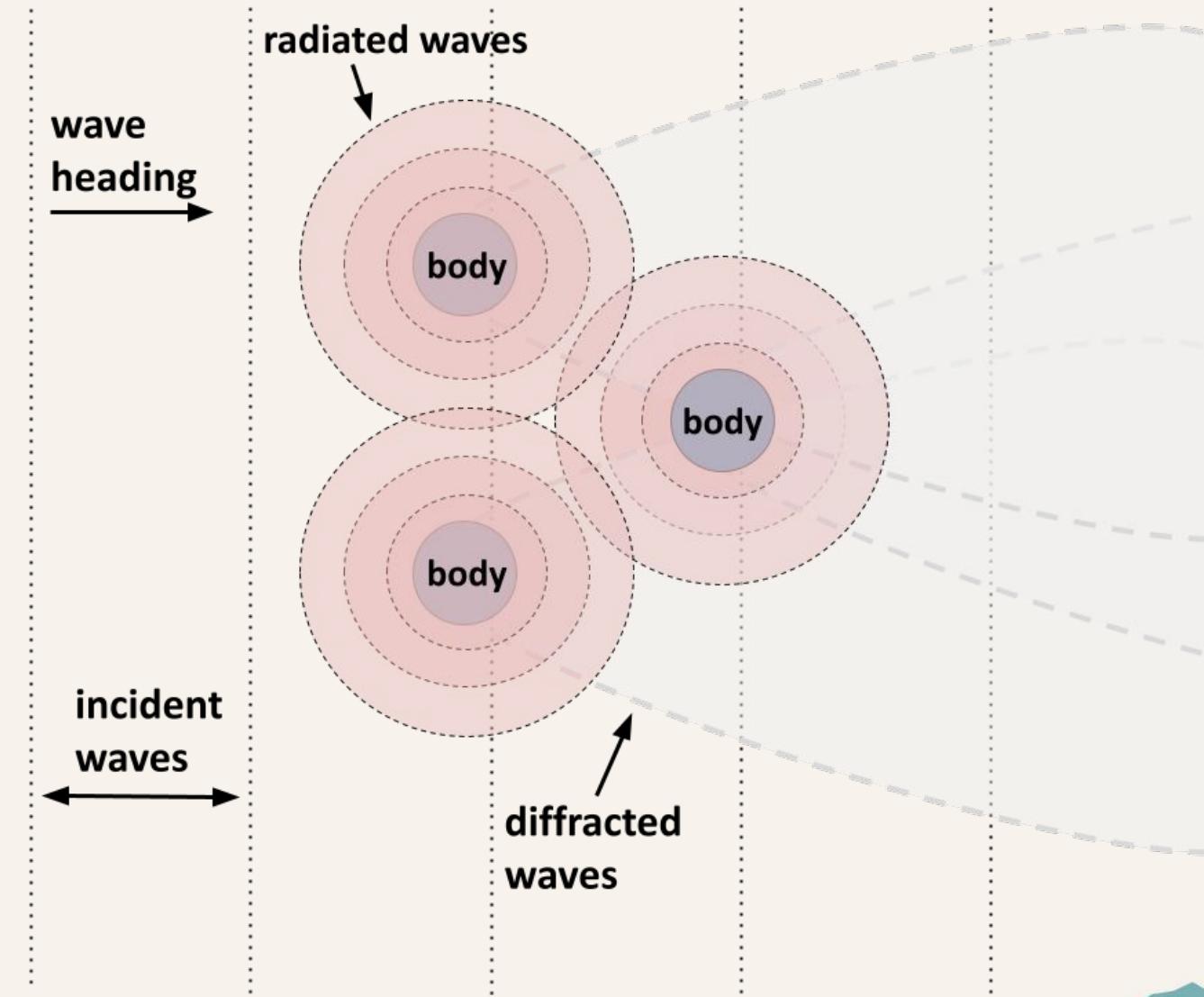


Results → Single

# Methodology → Arrays

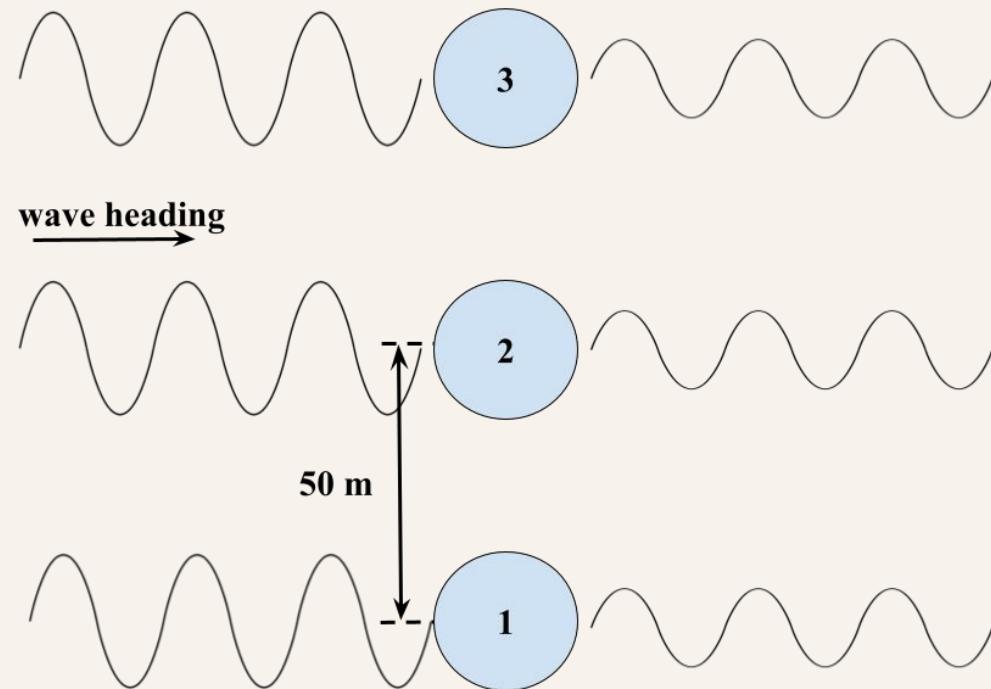
Oscillating bodies can interact in ways that are constructive or destructive to power production<sup>[22,23]</sup>

- does this correspond to their wave sheltering performance?

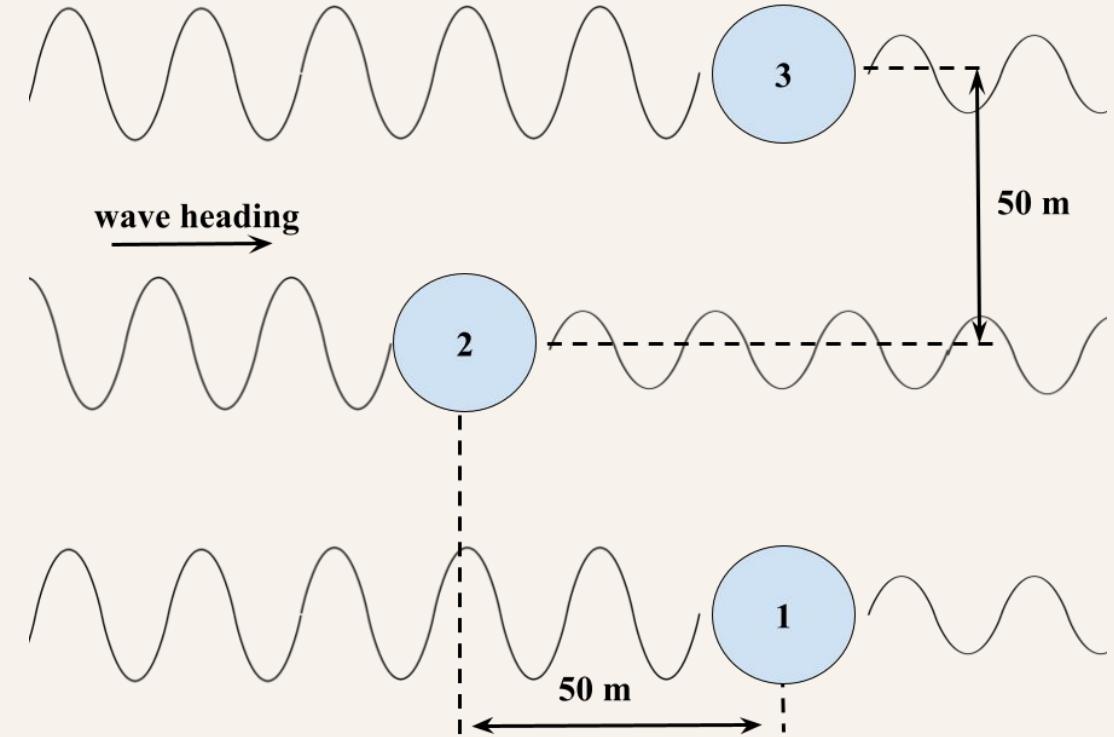


# Methodology → Arrays

We model two arbitrary, non-optimized array configurations



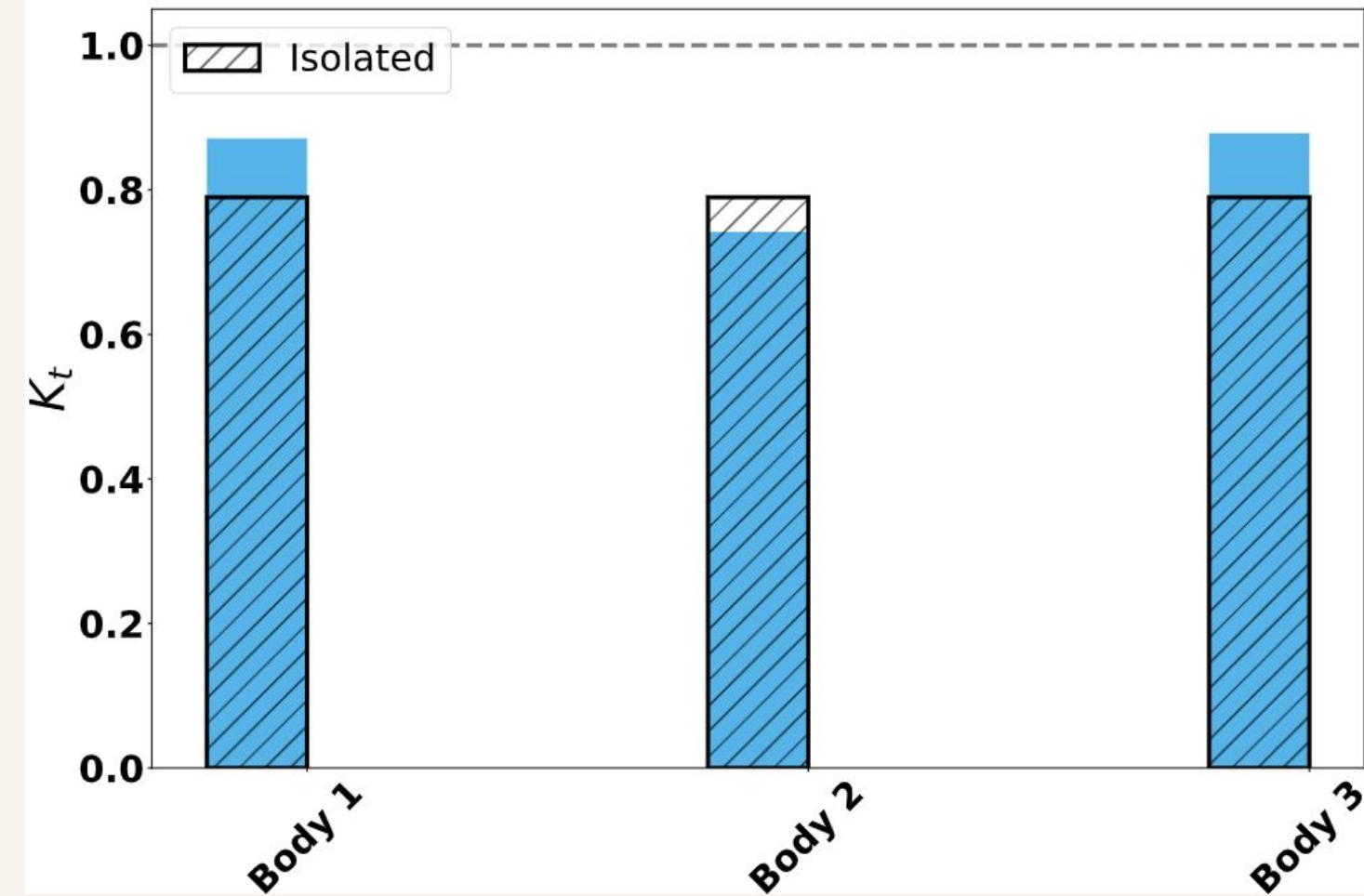
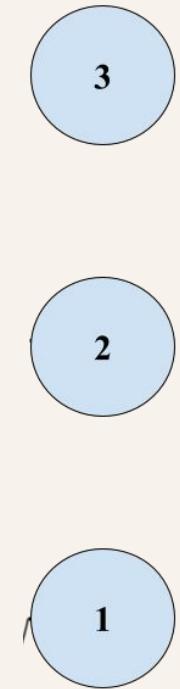
Regular



Staggered

# Breakwater

The sheltering effect is **concentrated in the center**, with the periphery experiencing less wave sheltering



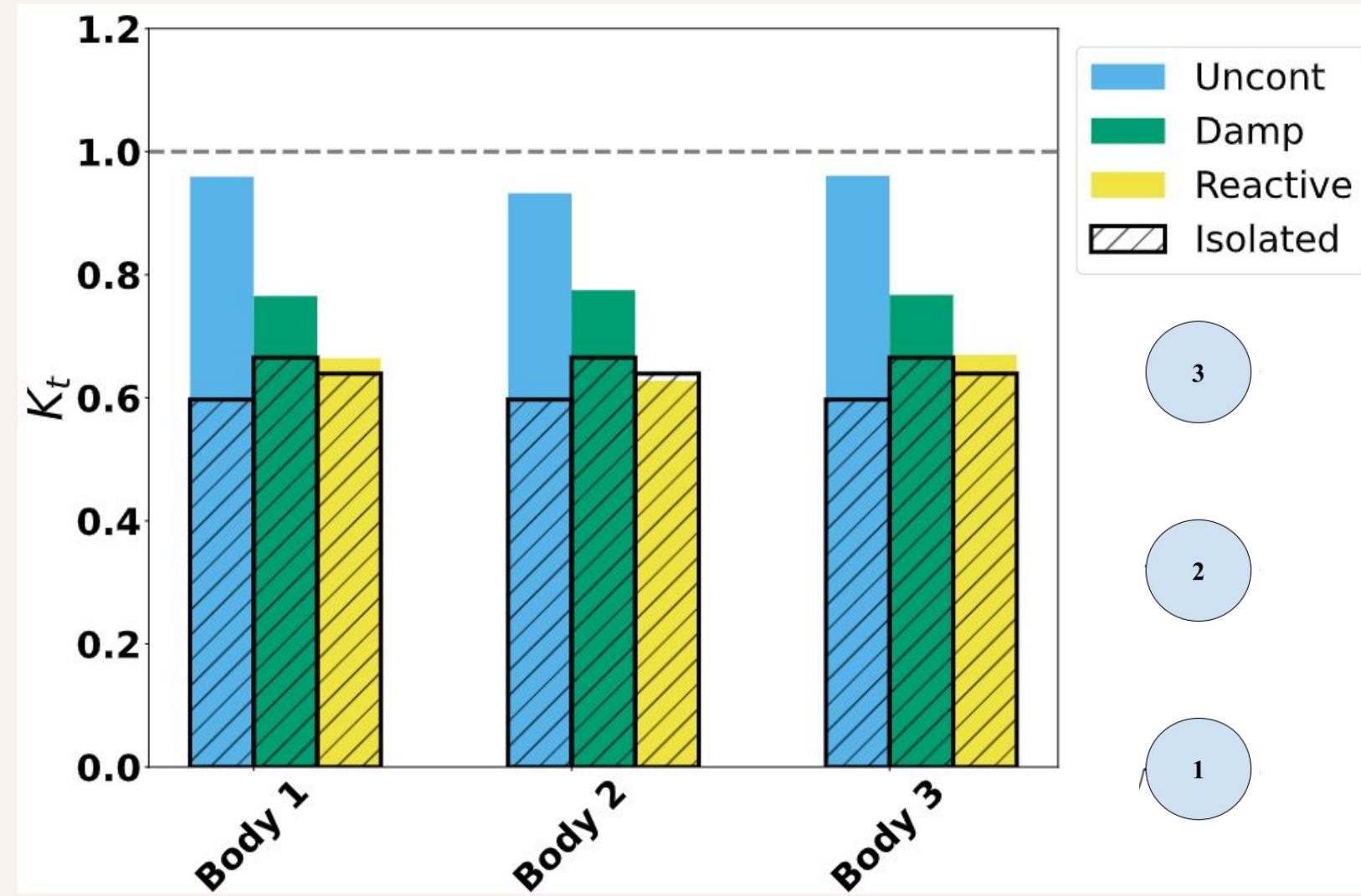
\*at a frequency of 1.25 rad/s

Results → Array (Regular)

# Results → Array (Regular) OSWEC

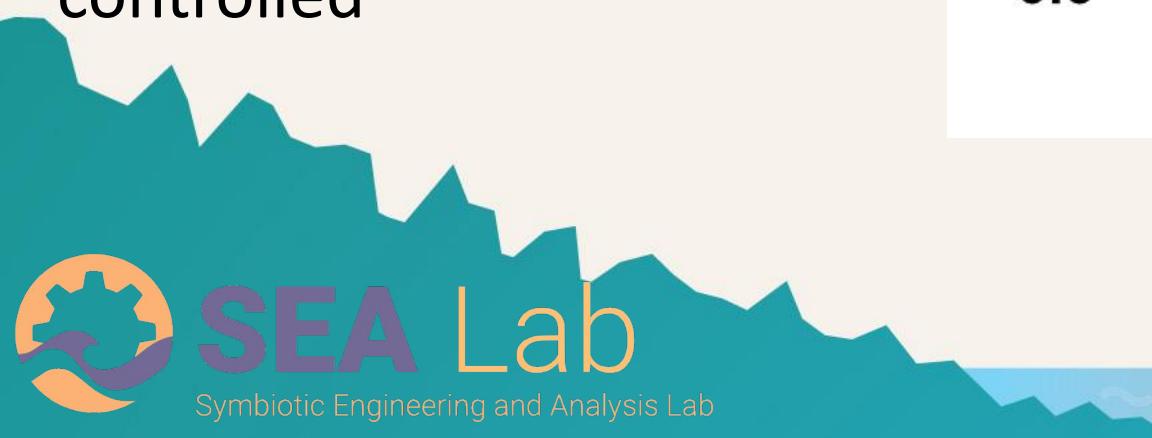
We see modeling the body in isolation is **underpredicting wave transmission** for the uncontrolled and damped cases

There is **little change** when the bodies are reactively controlled



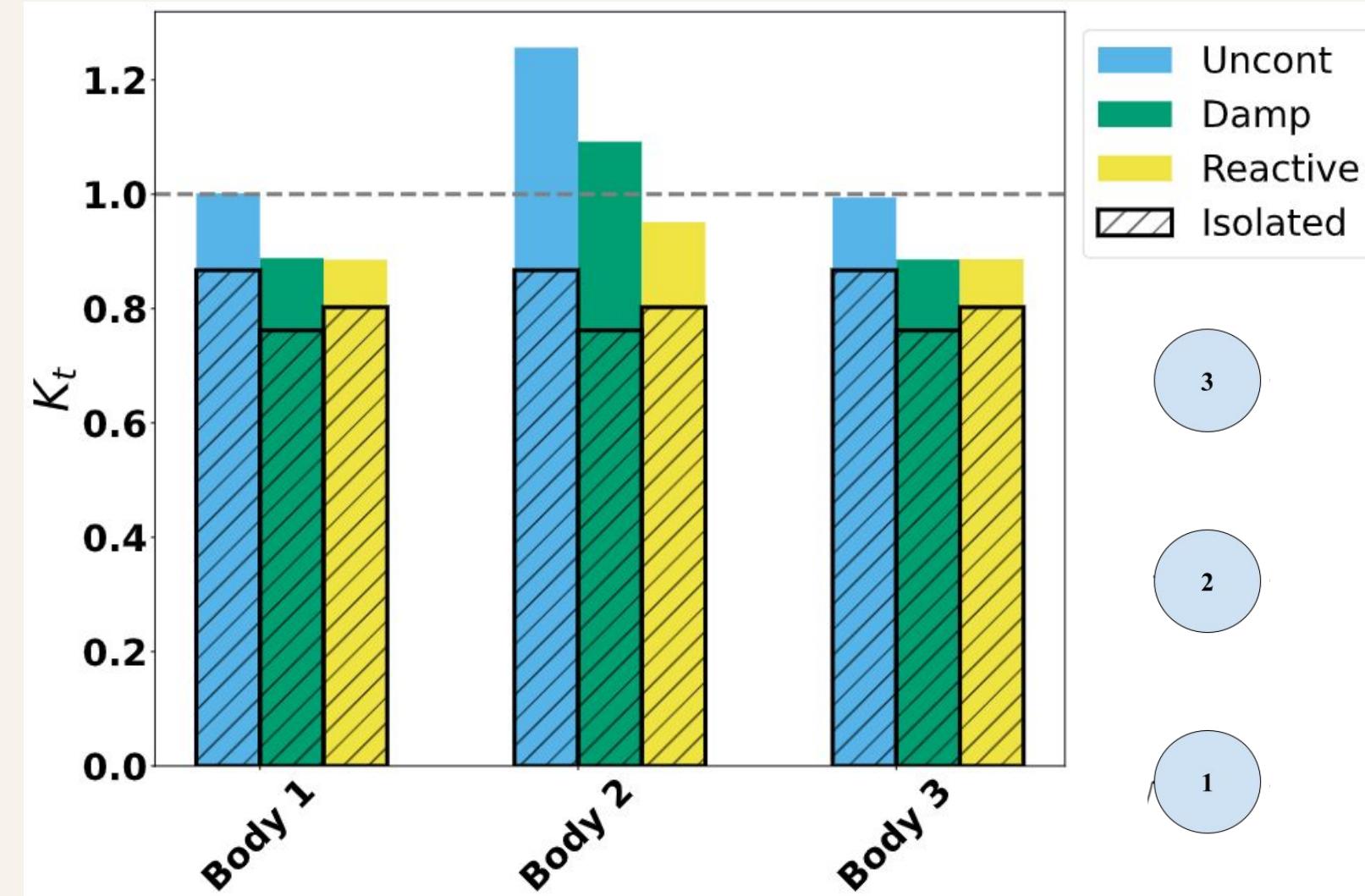
\*at a frequency of 1.25 rad/s

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# Results → Array (Regular) Point Absorber

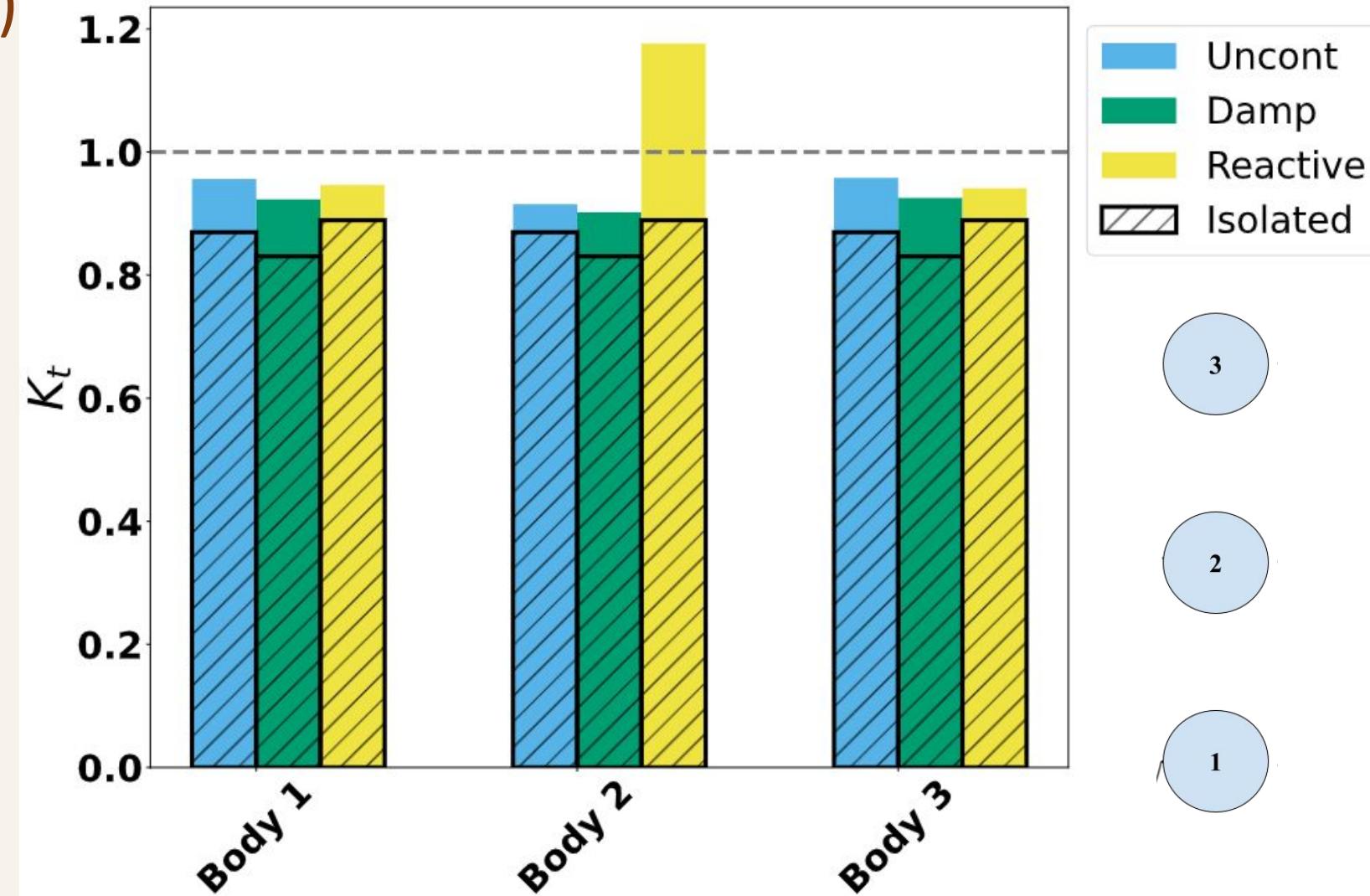
We see the **wave sheltering of Body 2 negated by interactions of Bodies 1 and 3** in the damped control case.



\*at a frequency of 1.25 rad/s

# Results → Array (Regular) Attenuator

We see a **slight underprediction** and again energy balance violation with reactive control



\*at a frequency of 1.25 rad/s

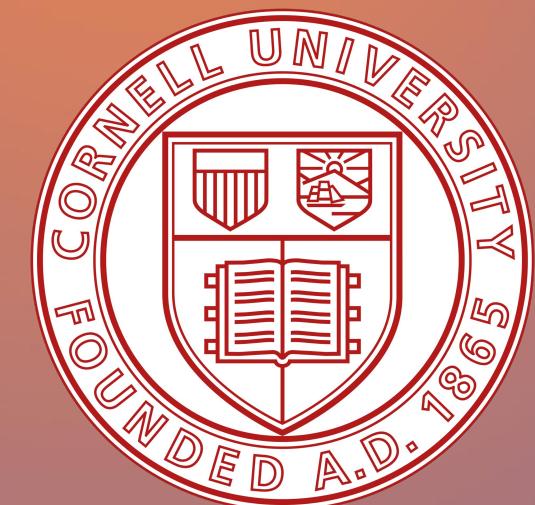
# Conclusions

1. We defined WEC **wave sheltering capabilities by their fluid-structure interactions** ( $K_t$  and  $K_r$ )
2. We determined the **OSWEC architecture** had the lowest wave transmission across frequencies and the **breakwater typically outperforms the PA and attenuator**
3. We saw that wave sheltering performance can be **affected by array interactions**, but the extent to which this is relevant in the far field needs further investigation

# Acknowledgements



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# Thank You! Questions?

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GitHub (to be released):  
<https://github.com/symbiotic-engineering/transmission-reflection>



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